

6/3/25

Washington State Department of Transportation

RE: Existing Box Culvert Evaluation

As part of the I-405, SR522 Vicinity to SR527 Express Toll Lanes Improvement Project, traffic from the I-405 will be shifted onto an existing concrete box culvert located in the median. The existing culvert was built in 1996. Since the available plans for the culvert do not match field conditions, the following information was determined based on field investigation:

- Configuration and materials: Single-cell precast concrete box culvert
- Geometry: Interior dimensions are 20' wide x 9' high, with 2' chamfer at top and bottom. Wall and slab thicknesses are 10".
- Depth of fill above culvert: Varies from 4'-6'
- Reinforcement:
  - Top Slab - Interior: #7 bars at 5" o.c. transverse and #5 bars at 10" o.c. longitudinal
  - Wall – Interior: #5 bars at 5" o.c. vertical with #5 bars at 10" o.c. horizontal
  - Wall – Exterior: #7 bars at 5" o.c. vertical with #5 bars at 10" o.c. horizontal

In order to analyze the culvert, the below assumptions were made:

- Concrete strength,  $f'_c = 5000$  psi. Typical for precast concrete.
- Reinforcing steel strength,  $f_y = 60,000$  psi
- Fill density above culvert: 127 pcf. This is a weighted average which includes 6" of asphalt at 140 pcf with compacted or saturated soils below at 125 pcf.
- Reinforcement:
  - Corner bars are assumed equivalent to vertical exterior wall bars (#7 at 5" o.c.) as is standard practice. These bars are often combined into one single U-shaped bar.
  - Bottom slab reinforcement is taken to be equal to the top slab reinforcement. Standard practice is equivalent or better.
  - Top and bottom slab exterior reinforcement is taken to be #5 bars at 10" o.c. in both directions, matching the top slab longitudinal rebar and the horizontal wall rebar. Standard practice is equivalent or better.
  - Additional bars were added around the riser/access openings, to account for the opening, which provide the same level of strength as uninterrupted bars. This assumption is based on typical details for openings in similar box culverts (provided on Page 75).

The culvert parameters outlined above were analyzed in the Eriksson Culvert software, the program indicated for box culvert design and analysis per the WSDOT Bridge Design Manual (BDM). The software inputs can be viewed on Pages 5-6. Input values that were confirmed by field investigations are highlighted for reference.

To evaluate the ability of the culvert to support traffic loading, load ratings were determined for HL-93 loads and the additional rating trucks outlined in Chapter 13 of the BDM. It was determined that the culvert

could support the various truck loadings with ratings greater than 1.0 for all loadings except HL-93 (see Page 9). Although there are two lanes of traffic above the culvert running parallel to the centerline of the culvert, one of these lanes is an express lane and not likely to be subject to truck loadings. However, to ensure HL-93 truck loadings could be supported in both lanes simultaneously, temporary shoring has been conservatively added to the center of the culvert. The shoring is designed to carry the HL-93 Live Load only. To approximate load ratings for this condition, the culvert was modeled as a double box culvert with a center stem. The corresponding load ratings can be found on Pages 3 and 22. Minimum controlling HL-93 inventory and operating ratings are 1.26 and 1.63 respectively, demonstrating that the culvert can safely support the worst-case traffic loadings which could occur during construction.

Additionally, the concrete riser and steel plate cover strength was evaluated under HL-93 LL and soil DL and found to be acceptable (see Pages 36-39).



6-3-25

**BRIDGE RATING SUMMARY:  
EXISTING CULVERT (WITH SHORING)**



6-3-25

Bridge Name: Drainage Vault  
 Bridge Number: V001  
 SID Number: XG180500  
 Span Types: N/A  
 Bridge Length: 285 ft  
 Design Load: HL-93  
 Engineering Firm/Agency: 4M Engineering  
 Rated By: Jessica Merrell  
 Checked By: Forrest Megargel  
 Date: 6/3/2025

Inspection Report Date:	3/13/2025	Deck Condition	N/A
Rating Method:	LRFR	Superstructure Condition	N/A
Overlay Thickness:	N/A	Substructure Condition	N/A

<b>Truck</b>	<b>RF</b>	<b>γ</b>	<b>Controlling Point</b>
AASHTO 1 (Type 3)	2.08	2.0	Shear @ bottom slab
AASHTO 2 (Type 3S2)	2.28	2.0	Shear @ bottom slab
AASHTO 3 (Type 3-3)	2.21	2.0	Shear @ bottom slab
Legal Lane	2.73	2.0	Shear @ bottom slab
NRL	2.08	2.0	Shear @ bottom slab
LGL-105	2.08	2.0	Shear @ bottom slab
OL-1	3.44	1.20	Shear @ top slab
OL-2	3.36	1.20	Shear @ top slab
EV2	2.04	1.30	Shear @ top slab
EV3	2.20	1.30	Shear @ top slab

<b>SNBI Rating</b>	<b>RF</b>	<b>γ</b>	<b>Controlling Point</b>
Inventory (HL-93)	1.26	1.75	Shear @ bottom slab
Operating (HL-93)	1.63	1.35	Shear @ bottom slab

**Remarks:**

Per inspection report, concrete culvert is 20'x9' in good condition.

---

*Existing Culvert Analysis  
(Unshored)*

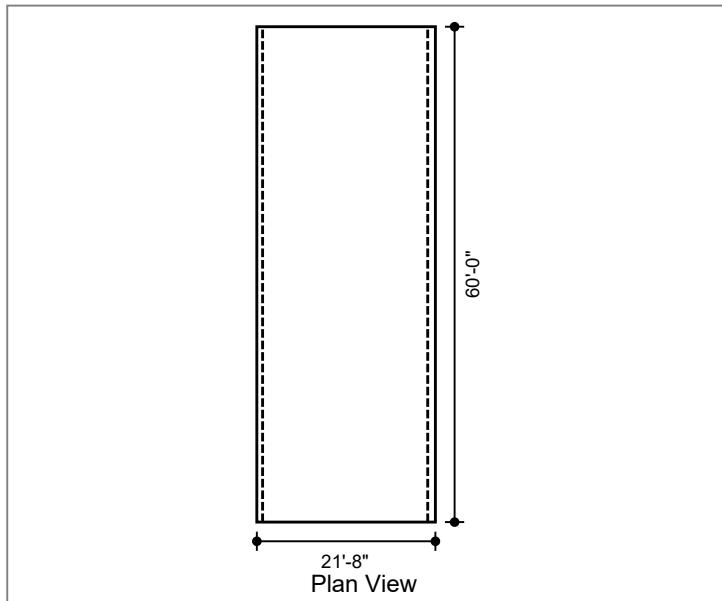
---

Project : Bothell to Swamp Creek  
 Task : Box Culvert Evaluation  
 Job No. : \_\_\_\_\_  
 Client: Skanska  
 File: Bothell Culvert Analysis 522.etcx

Spec.: LRFD 9th ed.  
 Type of Culvert: Precast

**Physical Dimensions**

Clear Span: 20'-0"  
 Clear Height: 9'-0"  
 Top Slab: 10"  
 Bottom Slab: 10"  
 Ext. Wall: 10"  
 Fill Depth Range  
 Maximum: 6.00 ft  
 Minimum: 4.00 ft  
 Increment: 0.50 ft  
 Length: 60'-0"  
 Skew Angle: 0.00 deg  
 Bottom Slab Support: Full Slab  
 Top Haunch, Width: 2'-0"  
 Top Haunch, Height: 2'-0"  
 Bottom Haunch, Width: 2'-0"  
 Bottom Haunch, Height: 2'-0"



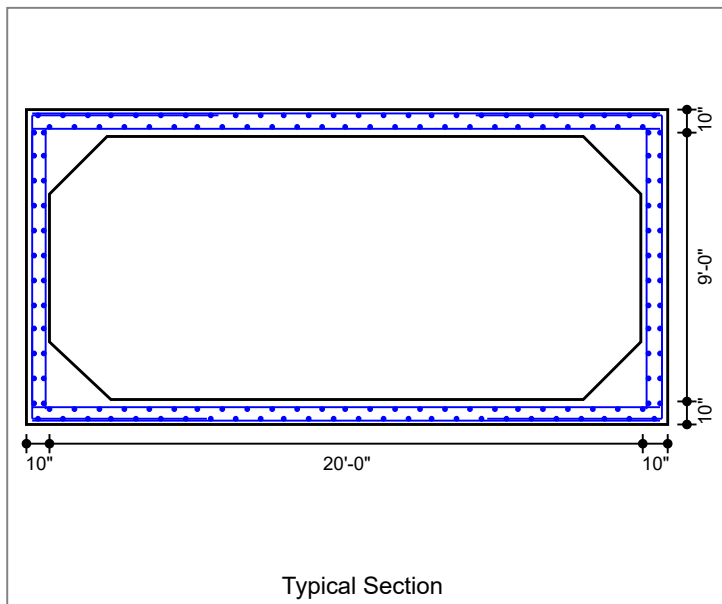
**Material Properties**

**Concrete**  
 Strength, f'c: 5.000 ksi  
 Density: 0.155 kcf  
 Elasticity, Ec: 4903 ksi  
 Type: Normal wt

**Steel**  
 Yield, fy: 60 ksi  
 Allow Stress: 36 ksi  
 Elasticity, Es: 29000 ksi

**Soil**  
 Density: 0.127 kcf  
 Exposure Factor  
 User-Defined: 1.00

**Reinforcement Covers**  
 Ext. Cover Top Slab: 2"  
 Ext. Cover Bottom Slab: 2"  
 Ext. Cover Walls: 2"  
 Int. Cover Walls: 2"  
 Int. Cover Top Slab: 2"  
 Int. Cover Bottom Slab: 2"



**Controlling Ratings**

Inventory Rating: 0.75  
 Operating Rating: 0.97

**Loads**

**Live Load**  
 Vehicle Names: HL-93, Type 3S2, Overload 2, NRL - Legal Lane, NRL, Type 3-3, EV 2, WA-105, Type 3, Overload 1, EV 3  
 Traffic Direction: Perpendicular  
 Eq. Height of Soil: Calculated  
 Max No. of Lanes: 2

**Dead Load**  
 Future Wearing Surface: 0.000 klf  
 Additional Dead Load: 0.000 klf  
 Concentrated Loads: none

**Lateral Soil Loads**  
 Eq. Fluid Press. Max: 60.00 pcf  
 Eq. Fluid Press. Min: 30.00 pcf

Interior Water Pressure: no  
 Exterior Water Pressure: no

Project : Bothell to Swamp Creek  
 Task : Box Culvert Evaluation  
 Job No. :

Client: Skanska  
 File: Bothell Culvert Analysis 522.etcx

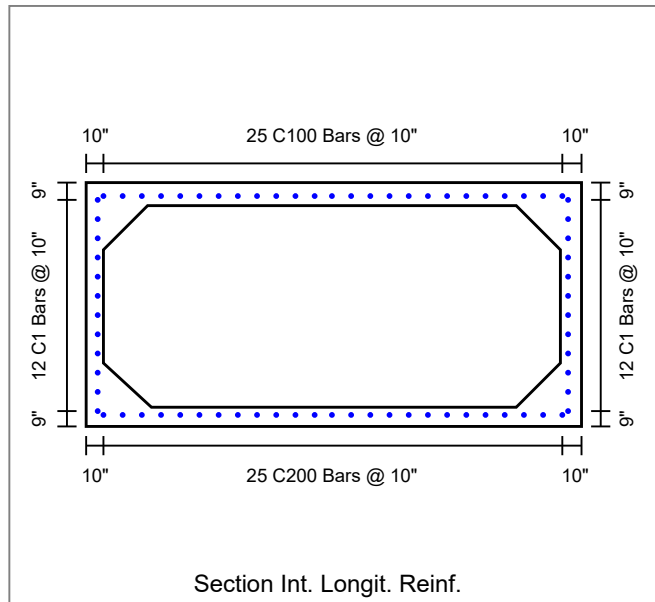
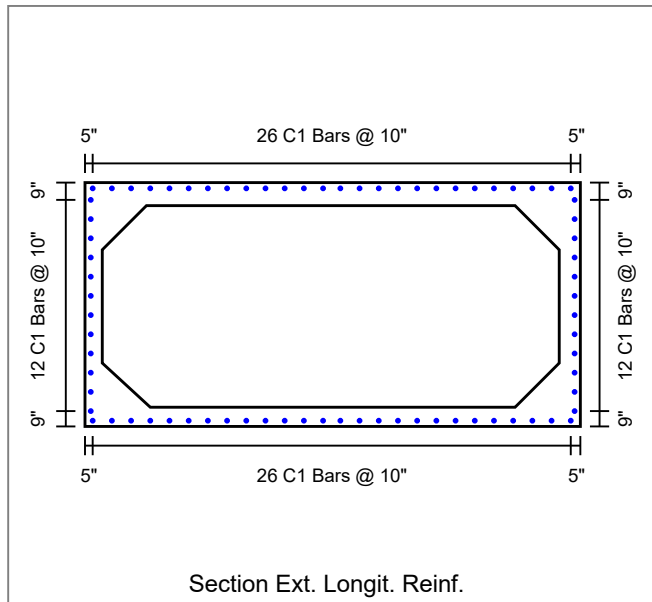
Sht \_\_\_\_\_ of \_\_\_\_\_  
 By: \_\_\_\_\_  
 Ck: \_\_\_\_\_  
 5/23/2025 2:47:20 PM  
 p. 2 of 4

**Concrete Summary**

Volume of Concrete: 2.189 cy/ft Total Volume of Concrete: 131.358 cy

**Reinforcing Steel Bar Schedule (lb)**

Location	Mark	Qty	Size	Spacing	Type	Length	Hor.Leg	Ver.Leg	Tot.Weight
Top Slab(Int)	A100 (AS2)	144	7	5"	S	21'-3"	--	--	6255.0
Bot Slab(Int)	A200 (AS3)	144	7	5"	S	21'-3"	--	--	6255.0
Top Slab(Ext)	A300 (AS7)	72	5	10"	S	21'-3"	--	--	1596.0
Bot Slab(Ext)	A400 (AS8)	72	5	10"	S	21'-3"	--	--	1596.0
Corner(Top)	A1 (AS1)	288	7	5"	L	9'-5"	6'-4"	3'-1"	5543.0
Corner(Bot)	A2 (AS1)	288	7	5"	L	9'-0"	5'-11"	3'-1"	5298.0
Wall(Int)	B1 (AS4)	288	5	5"	S	9'-6"	--	--	2854.0
Wall(Ext)	B2 (AS1)	288	7	5"	S	9'-0"	--	--	5298.0
Longit. Top (Int)	C100 (AS5)	25	5	10"	S	59'-11"	--	--	1562.0
Longit. Bot (Int)	C200	25	5	10"	S	59'-11"	--	--	1562.0
Longit. Top (Ext)	C1 (AS6)	26	5	10"	S	59'-11"	--	--	1624.7
Longit. Bot (Ext)	C1 (AS6)	26	5	10"	S	59'-11"	--	--	1624.7
Longit. Wall (Ext)	C1 (AS6)	24	5	10"	S	59'-11"	--	--	1499.8
Longit. Wall (Int)	C1 (AS6)	24	5	10"	S	59'-11"	--	--	1499.8
									44068



**Notes:**  
 -Field verified values are highlighted.  
 -A1, A2, and B2 are often combined into one U-bar, or same sizes used. A1 and A2 are assumed to match B2.  
 -Bottom slab interior rebar typically matches or exceeds top slab interior rebar (assumed to match top slab rebar)  
 -Other bars are conservatively assumed to be #5 @ 10" o.c.

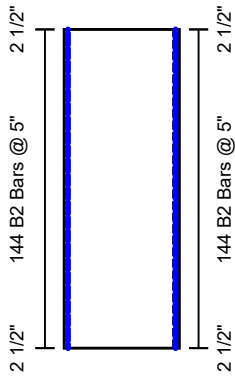
Project : Bothell to Swamp Creek

Task : Box Culvert Evaluation

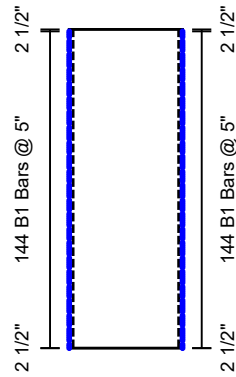
Job No. :

Client: Skanska

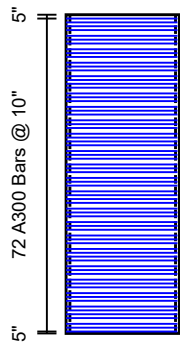
File: Bothell Culvert Analysis 522.etcx



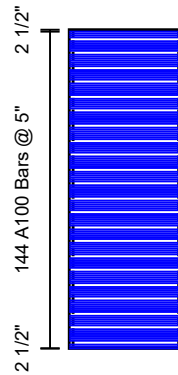
Ext. Wall Reinf.



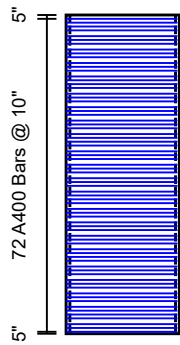
Int. Wall Reinf.



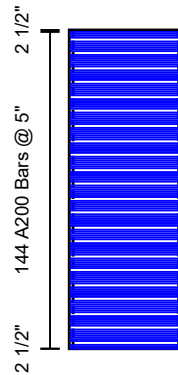
Top Slab Ext. Reinf.



Top Slab Int. Reinf.



Bottom Slab Ext. Reinf.



Bottom Slab Int. Reinf.

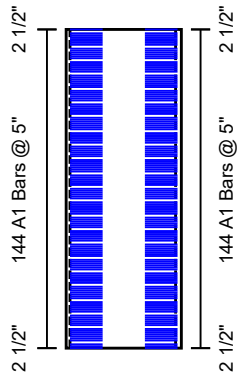
Project : Bothell to Swamp Creek

Task : Box Culvert Evaluation

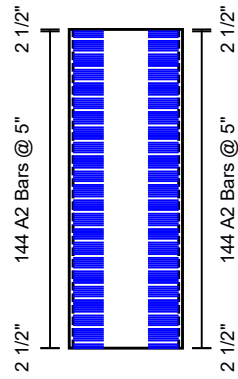
Job No. :

Client: Skanska

File: Bothell Culvert Analysis 522.etcx



Top Slab Corner Reinf.



Bottom Slab Corner Reinf.

RATINGS SUMMARY  
 =====

Truck	Flexure			Shear		
	RF(INV)	RF(OP)	Controlling Point	RF(INV)	RF(OP)	Controlling Point
(AA) HL-93	0.75	0.97	Ext wall, BOT	0.83	1.08	Bottom Slab, RT
(AB) NRL	1.17	1.17	Ext wall, BOT	1.37	1.37	Bottom Slab, LT
(AC) Type 3	1.17	1.17	Ext wall, BOT	1.37	1.37	Bottom Slab, LT
(AD) Type 3S2	1.27	1.27	Ext wall, BOT	1.50	1.50	Bottom Slab, LT
(AE) Type 3-3	1.24	1.24	Ext wall, BOT	1.45	1.45	Bottom Slab, LT
(AF) Overload	2.11	2.11	Ext wall, BOT	2.56	2.56	Top Slab, LT
(AG) Overload	2.06	2.06	Ext wall, BOT	2.50	2.50	Top Slab, LT
(AH) EV 2	1.29	1.29	Ext wall, BOT	1.54	1.54	Top Slab, RT
(AI) EV 3	1.38	1.38	Ext wall, BOT	1.64	1.64	Top Slab, LT
(AJ) NRL - Le	1.47	1.47	Ext wall, BOT	1.74	1.74	Bottom Slab, LT
(AK) WA-105	1.17	1.17	Ext wall, BOT	1.37	1.37	Bottom Slab, LT

REINFORCEMENT SUMMARY  
 =====

M dimension = 5' 3" (method of equivalent capacity)  
 = 6' 12" (method of contraflexure - ASTM)

Reinforcing steel Schedule  
 -----

Location	Bar Mark	Qty	Size	Type	Spacing (in)	As,prv (in2/ft)	Length (ft-in)	Wgt (lbs)	H Leg (ft-in)	V Leg (ft-in)
Top slab (int)	A100 (AS2)	144	7	STR	5.00	1.440	21- 3	6255		
Bot slab (int)	A200 (AS3)	144	7	STR	5.00	1.440	21- 3	6255		
Top slab (ext)	A300 (AS7)	72	5	STR	10.00	0.372	21- 3	1596		
Bot slab (ext)	A400 (AS8)	72	5	STR	10.00	0.372	21- 3	1596		
Corner (Top)	A1 (AS1)	288	7	L-BAR	5.00	1.440	9- 5	5543	6- 4	3- 1
Corner (Bottom)	A2 (AS1)	288	7	L-BAR	5.00	1.440	9- 0	5298	5-11	3- 1
Ext wall (int)	B1 (AS4)	288	5	STR	5.00	0.744	9- 6	2854		
Ext wall (ext)	B2 (AS1)	288	7	STR	5.00	1.440	9- 0	5298		
Top slab (int- 1)	C100 (AS5)	25	5	STR	10.00	0.372	59-11	1562		
Bot slab (int- 1)	C200	25	5	STR	10.00	0.372	59-11	1562		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Total								44068		

Note: A denotes flexural steel, B denotes vertical steel, C denotes longitudinal steel

AS Bar Marks  
 -----

Location	As prv in2/ft
Transverse Side Wall - Outside Face (AS1)	1.440
Transverse Top Slab - Inside Face (AS2)	1.440
Transverse Bottom Slab - Inside Face (AS3)	1.440
Transverse Side Wall - Inside Face (AS4)	0.744
Distribution Top Slab - Inside Face (AS5)	0.372
Distribution Top Slab - Outside Face (AS6)	0.372
Transverse Top Slab - Outside Face (AS7)	0.372
Transverse Bottom Slab - Outside Face (AS8)	0.372

Notes: 1.) Final areas of steel provided must be checked in analysis mode

Project: Bothell to Swamp Creek  
 Task : Box Culvert Evaluation  
 Client : Skanska  
 Job No.:

CULVERT PROPERTIES

=====  
 Type of Culvert: Precast Specification : LRFD 9th Edition  
 Operating Mode : Analysis

Physical Dimensions

-----  
 No. of Boxes: 1 Name: BoxCulvert  
 Clear Span : 20.0000 ft  
 Clear Height: 9.0000 ft Skew Angle : 0.00 deg  
 Length : 60.0000 ft Bottom Slab Support: Full Slab  
 Fill Depth Range: Maximum : 6.00 ft Minimum : 4.00 ft Increment : 0.50 ft  
 Haunches: Top, Length: 24.0000 in Height: 24.0000 in  
 Bottom, Length: 24.0000 in Height: 24.0000 in  
 Member Thicknesses: Top Slab: 10.0000 in Bot Slab: 10.0000 in  
 Ext wall: 10.0000 in

Wall Joint: None

Material Properties

-----  
 Concrete: Strength, f'c : 5.000 ksi Density : 0.155 kcf Elasticity, Ec: 4903 ksi  
 Type : Normal weight Density Modification Factor : 1.00  
 Fr Factor : 0.24 Gamma1 : 1.60 Gamma3 : 1.00 (user defined)  
 Steel: Yield, fy : 60.00 ksi fss Limit : 0.60fy Elasticity, Es: 29000 ksi  
 Yield, fyv : 60.00 ksi Diameter : 1.000 in Type : Rebar  
 Soil: Density : 0.127 kcf Slope Factor: 1.150  
 Poisson's : 0.5  
 Fe Factor : 1.000 (User Defined)  
 Serviceability, Gamma-e: 1.00

Loads

-----  
 Live Load: Vehicle: (AA) HL-93 - Design Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 8.00 0.00  
 2 32.00 14.00  
 3 32.00 14.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: yes  
 Tandem: Axle 1: 25.00 k, Axle 2: 25.00 k, Axle Spacing: 4.00 ft  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Inventory Rating Load Factor: 1.75 Operating Rating Load Factor: 1.35  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no  
 Vehicle: (AB) NRL - Legal Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 8.00 0.00  
 2 8.00 4.00  
 3 8.00 4.00  
 4 17.00 4.00  
 5 17.00 4.00  
 6 8.00 4.00  
 7 8.00 4.00  
 8 6.00 6.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no  
 Vehicle: (AC) Type 3 - Legal Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 17.00 0.00  
 2 17.00 4.00  
 3 16.00 15.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I

Override MPF: no  
Override DLA: no  
Vehicle: (AD) Type 3S2 - Legal Vehicle  
Axle No. weight(k) Dist. From Previous(ft)  
1 15.50 0.00  
2 15.50 4.00  
3 15.50 22.00  
4 15.50 4.00  
5 10.00 11.00  
Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 2  
Design Load Combinations: Strength I  
Override MPF: no  
Override DLA: no

Vehicle: (AE) Type 3-3 - Legal Vehicle  
Axle No. weight(k) Dist. From Previous(ft)  
1 14.00 0.00  
2 14.00 4.00  
3 16.00 16.00  
4 12.00 15.00  
5 12.00 4.00  
6 12.00 15.00  
Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 2  
Design Load Combinations: Strength I  
Override MPF: no  
Override DLA: no

Vehicle: (AF) Overload 1 - Permit Vehicle  
Axle No. weight(k) Dist. From Previous(ft)  
1 21.50 0.00  
2 21.50 4.00  
3 21.50 12.00  
4 21.50 4.00  
5 10.00 10.00  
Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 1.2  
Design Load Combinations: Strength II  
Override MPF: no  
Override DLA: no

Vehicle: (AG) Overload 2 - Permit Vehicle  
Axle No. weight(k) Dist. From Previous(ft)  
1 22.00 0.00  
2 21.50 6.00  
3 21.50 4.00  
4 22.00 14.00  
5 21.50 6.00  
6 21.50 4.00  
7 22.00 16.00  
8 21.50 6.00  
9 21.50 4.00  
10 12.00 10.00  
Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 1.2  
Design Load Combinations: Strength II  
Override MPF: no  
Override DLA: no

Vehicle: (AH) EV 2 - Permit Vehicle  
Axle No. weight(k) Dist. From Previous(ft)  
1 24.00 0.00  
2 33.50 15.00  
Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck Or Tandem Or Lane  
Rating Load Factor: 1.3  
Design Load Combinations: Strength II  
Override MPF: no  
Override DLA: no

Vehicle: (AI) EV 3 - Permit Vehicle  
Axle No. weight(k) Dist. From Previous(ft)

1 24.00 0.00  
 2 31.00 15.00  
 3 31.00 4.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck Or Tandem Or Lane  
 Rating Load Factor: 1.3  
 Design Load Combinations: Strength II  
 Override MPF: no  
 Override DLA: no

Vehicle: (AJ) NRL - Legal Lane - Legal Vehicle

Axle No.	Weight(k)	Dist. From Previous(ft)
1	10.50	0.00
2	10.50	4.00
3	12.00	16.00
4	9.00	15.00
5	9.00	4.00
6	9.00	15.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.20 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no

Vehicle: (AK) WA-105 - Legal Vehicle

Axle No.	Weight(k)	Dist. From Previous(ft)
1	14.00	0.00
2	14.00	4.00
3	17.00	10.00
4	17.00	32.00
5	17.00	4.00
6	7.00	4.00
7	7.00	4.00
8	12.50	11.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no

Include Lane Load : yes Max. No. of Lanes: 2  
 Traffic Direction : Lanes Perpendicular to Main Reinforcement  
 Neglect Live Load if: Fill > 8 ft and Fill > Clear Span  
 Apply Surcharge at Fill Depths > 2 ft : yes  
 Compute Surcharge Depth: yes

Dead Load: Future wearing Surface : 0.00 klf Add. Dead Load : 0.00 klf  
 Concentrated Loads : none

Lateral Soil Loads: Max. Equiv. Fluid Press.: 60.00 pcf Min. Equiv. Fluid Press. : 30.00 pcf

Include Additional Uniform Horiz. Load: no  
 Include Additional Uniform Vert. Load: no  
 Buoyancy Check : no  
 Fluid Pressures : Apply Water Press. : no  
 Foundation Model : Uniform Loads  
 Seismic Analysis : Do not include

Load and Resistance Factors

	Max	Min
DC:	1.250	0.900
DW:	1.500	0.650
EV:	1.300	0.900
EH:	1.350	0.900
WA:	1.000	
EQ:	1.000	
LL I :	1.750	LL II : 1.350
Ductility:	1.000	Importance: 1.000
Condition:	1.000	System : 1.000
Phi Shear:	0.900	Phi Moment: 1.000
PM Compression:	0.750	PM Tension : 0.900
Load Factor Multipliers, Design Mode:	1.00	Analysis Mode: 1.00

Reinforcement

Reinforcement Covers :	Exterior	Interior
Top Slab:	2.0000 in	2.0000 in
walls :	2.0000 in	2.0000 in
Bot Slab:	2.0000 in	2.0000 in

Assigned reinforcement:

Location	Mark	Size	Spacing (in)
Top Slab Inside	A100 (AS2)	7	5.0000
Bottom Slab Inside	A200 (AS3)	7	5.0000
Top Slab Outside	A300 (AS7)	5	10.0000
Bottom Slab Outside	A400 (AS8)	5	10.0000
Top Corner	A1 (AS1)	7	5.0000
Bottom Corner	A2 (AS1)	7	5.0000
Ext. Wall Inside	B1 (AS4)	5	5.0000
Ext. wall Outside	B2 (AS1)	7	5.0000
Longitudinal	C1 (AS6)	5	10.0000
Top Distribution	C100 (AS5)	5	10.0000
Bottom Distribution	C200	5	10.0000

Analysis Options

```

-----
LL Analysis      : Automatically Set Traffic Direction to Account for Skew Effects: no
                  Limit LL Distribution Width to Culvert Length for: None
                  Combine Longitudinal Axle Distribution Overlaps: No
                  Combine Transverse Axle Distribution Overlaps: No
                  Axle Placement Increment for Moving Load Analysis: 20
                  Include Impact on Bottom Slab: yes
                  Always Distribute wheel Load: yes
                  Deflection Criteria      : 1/800
                  Approach Slab will be Used: no
Reinforcement   : Always Include Distribution Steel: no
                  Distribution Slab Provided: no
                  User Defined Longitudinal Steel: yes
                  Max. As used in Vc Calcs: 2.00 in2/ft
                  Distribute Minimum Reinforcement per Face: yes
                  Use individual Member Thicknesses for Min Steel: no
                  Epoxy coat steel: no
                  Use M-dimension for bar length calcs.: no
Slenderness     : Checked      K Factor: 2.00
Analysis Modeling : Use Haunches in the Structural Analysis Model: yes
Critical Sections : Flexure critical section location: 1.5 member depth
                  Shear critical section location: dv beyond support
                  Use Max. Moment with Max. Shear at the Critical section for Shear: no
                  Include depth of haunch for critical sections: no
Flexure         : Ignore Axial Thrust: no
                  Use Eq. 12.10.4.2.4a-1: yes  Nu Multiplier: 1.00
Shear           : Always Check Iterative Beta Method
Environmental   : Apply durability factors: no
Load Combinations : LRFD min/min: no
    
```

ANALYSIS RESULTS  
 =====

Top Slab Thickness = 10.00 in  
 Bottom Slab Thickness = 10.00 in  
 Exterior Wall Thickness = 10.00 in

Modular Ratio (N) = 5.91 Max. Steel Ratio = 0.025  
 Design Span = 20.83 ft Design Height = 9.83 ft

Volume of Concrete: 2.189 cy/ft weight of Steel: 734 lb/ft

Note: Design and analysis results do not include force effects from stripping and handling stages

M dimension = 5' 3" (method of equivalent capacity)  
 = 6' 12" (method of contraflexure - ASTM)

Reinforcing Steel Schedule  
 -----

Location	Bar Mark	Qty	Size	Type	Spacing (in)	As,prv (in2/ft)	Length (ft-in)	Wgt (lbs)	H Leg (ft-in)	V Leg (ft-in)
Top Slab (int)	A100 (AS2)	144	7	STR	5.00	1.440	21- 3	6255		
Bot Slab (int)	A200 (AS3)	144	7	STR	5.00	1.440	21- 3	6255		
Top Slab (ext)	A300 (AS7)	72	5	STR	10.00	0.372	21- 3	1596		
Bot Slab (ext)	A400 (AS8)	72	5	STR	10.00	0.372	21- 3	1596		
Corner (Top)	A1 (AS1)	288	7	L-BAR	5.00	1.440	9- 5	5543	6- 4	3- 1
Corner (Bottom)	A2 (AS1)	288	7	L-BAR	5.00	1.440	9- 0	5298	5-11	3- 1
Ext wall (int)	B1 (AS4)	288	5	STR	5.00	0.744	9- 6	2854		
Ext wall (ext)	B2 (AS1)	288	7	STR	5.00	1.440	9- 0	5298		
Top slab (int- 1)	C100 (AS5)	25	5	STR	10.00	0.372	59-11	1562		
Bot slab (int- 1)	C200	25	5	STR	10.00	0.372	59-11	1562		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Total								44068		

Note: A denotes flexural steel, B denotes vertical steel, C denotes longitudinal steel

AS Bar Marks  
 -----

Location	As prv in2/ft
Transverse Side Wall - Outside Face (AS1)	1.440
Transverse Top Slab - Inside Face (AS2)	1.440
Transverse Bottom Slab - Inside Face (AS3)	1.440
Transverse Side Wall - Inside Face (AS4)	0.744
Distribution Top Slab - Inside Face (AS5)	0.372
Distribution Top Slab - Outside Face (AS6)	0.372
Transverse Top Slab - Outside Face (AS7)	0.372
Transverse Bottom Slab - Outside Face (AS8)	0.372

Notes: 1.) Final areas of steel provided must be checked in analysis mode

Summary of Ratings Table:  
 -----

Truck	Flexure								Shear				
	ILF	OLF	Fill	Member	Location	IR	OR	Fill	Member	Location	IR	OR	
(AA)HL-93	1.75	1.35	6.00	1	BOT	0.75	0.97	6.00	4	RT	0.83	1.08	
(AB)NRL	2.00	2.00	6.00	1	BOT	1.17	1.17	6.00	4	LT	1.37	1.37	
(AC)Type 3	2.00	2.00	6.00	1	BOT	1.17	1.17	6.00	4	LT	1.37	1.37	
(AD)Type 3	2.00	2.00	6.00	1	BOT	1.27	1.27	6.00	4	LT	1.50	1.50	
(AE)Type 3	2.00	2.00	6.00	1	BOT	1.24	1.24	6.00	4	LT	1.45	1.45	
(AF)overlo	1.20	1.20	6.00	1	BOT	2.11	2.11	4.00	2	LT	2.56	2.56	
(AG)overlo	1.20	1.20	6.00	1	BOT	2.06	2.06	4.00	2	LT	2.50	2.50	
(AH)EV 2	1.30	1.30	6.00	1	BOT	1.29	1.29	4.00	2	RT	1.54	1.54	
(AI)EV 3	1.30	1.30	6.00	1	BOT	1.38	1.38	4.00	2	LT	1.64	1.64	
(AJ)NRL -	2.00	2.00	6.00	1	BOT	1.47	1.47	6.00	4	LT	1.74	1.74	
(AK)WA-105	2.00	2.00	6.00	1	BOT	1.17	1.17	6.00	4	LT	1.37	1.37	

Critical Sections Summary: Flexure  
 -----

Member 1: (Exterior wall), Thickness = 10.00 in

Loc	Dist. (in)	Design Moment (k-ft)	Corr. A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)*	phi	As (in2)	Mcr (k-ft)	Load Ratings		Truck	Fill Depth (ft)
										IR	OR		
BOT	24.00	-58.07	19.07	48.35	7.56	53.31*	1.00	1.44	14.31	0.75	0.97	15AA	6.00

MID	59.00	0.00	6.37	26.97	7.69	29.13	1.00	0.74	14.31	NC	NC	AA	4.00
MID-	59.00	-55.33	19.07	48.35	7.56	53.31*	1.00	1.44	14.31	0.89	1.15	AA	6.00
TOP	24.00	-55.25	19.07	48.35	7.56	53.31*	1.00	1.44	14.31	0.90	1.17	AA	6.00

Member 2: (Top Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Moment (k-ft)	Corr. A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)	phi	As (in <sup>2</sup> )	Mcr (k-ft)	Load Ratings		Truck	Fill Depth (ft)
										IR	OR		
LT	24.00	-25.93	4.75	48.35	7.56	49.64	1.00	1.44	14.31	3.40	4.40	AA	6.00
MID	125.00	39.58	0.88	48.35	7.56	48.59	1.00	1.44	14.31	1.67	2.16	AA	6.00
MID-	125.00	0.37	4.49	13.89	7.69	15.58	1.00	0.37	14.31	NC	NC	AA	6.00
RT	24.00	-25.93	4.75	48.35	7.56	49.64	1.00	1.44	14.31	3.40	4.40	AA	6.00

Member 4: (Bottom Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Moment (k-ft)	Corr. A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)	phi	As (in <sup>2</sup> )	Mcr (k-ft)	Load Ratings		Truck	Fill Depth (ft)
										IR	OR		
LT	24.00	-28.60	7.42	48.35	7.56	50.35	1.00	1.44	14.31	3.70	4.79	AA	6.00
MID	125.00	41.27	2.89	48.35	7.56	49.14	1.00	1.44	14.31	1.63	2.12	AA	6.00
MID-	125.00	0.58	6.95	13.89	7.69	16.49	1.00	0.37	14.31	NC	NC	AA	6.00
RT	24.00	-28.60	7.42	48.35	7.56	50.35	1.00	1.44	14.31	3.70	4.79	AA	6.00

Critical Sections Summary: Vertical Shear

Member 1: (Exterior wall), Thickness = 10.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in <sup>2</sup> )	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
BOT	12.20	5.88	60.3	19.07	7.20	10.99	2.000	12.21 b	0.00	0.00	0.00	5.23	6.78	AA	6.00
MID	59.00	0.93	15.2	8.15	7.25	13.39	2.420	14.88 a	0.00	0.00	0.00	41.52	53.83	AA	5.50
MID-	59.00	0.29	51.0	16.59	7.20	10.99	2.000	12.21 b	0.00	0.00	0.00	13.61	17.64	AA	4.00
TOP	12.20	-3.93	56.1	19.07	7.20	10.99	2.000	12.21 b	0.00	0.00	0.00	4.80	6.22	AA	6.00

Member 2: (Top Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in <sup>2</sup> )	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
LT	12.20	17.13	42.3	4.75	7.56	17.31	n/a	19.24 c	0.00	0.00	0.00	1.03	1.34	AA	6.00
MID	125.00	2.03	36.5	0.35	7.56	17.31	n/a	19.24 c	0.00	0.00	0.00	8.52	11.04	AA	4.00
MID-	125.00	2.32	11.2	3.80	7.69	17.60	n/a	19.56 c	0.00	0.00	0.00	7.60	9.85	AA	4.00
RT	12.20	17.35	42.3	4.75	7.56	17.31*	n/a	19.24 c	0.00	0.00	0.00	0.99	1.29	AA	6.00

Member 4: (Bottom Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in <sup>2</sup> )	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
LT	12.20	17.86	46.5	7.42	7.56	17.31*	n/a	19.24 c	0.00	0.00	0.00	0.89	1.16	AA	6.00
MID	125.00	0.15	37.5	2.35	7.56	17.31	n/a	19.24 c	0.00	0.00	0.00	NC	NC	AA	4.00
MID-	125.00	0.17	0.0	6.25	7.69	23.39	5.052	25.99 a	0.00	0.00	0.00	NC	NC	AA	4.00
RT	12.20	18.24	46.5	7.42	7.56	17.31*	n/a	19.24 c	0.00	0.00	0.00	0.83	1.08	AA	6.00

Vc Calculation By: a - Iterative Beta, b - Constant Beta, c - Box Culvert, d - Standard/Arema

---

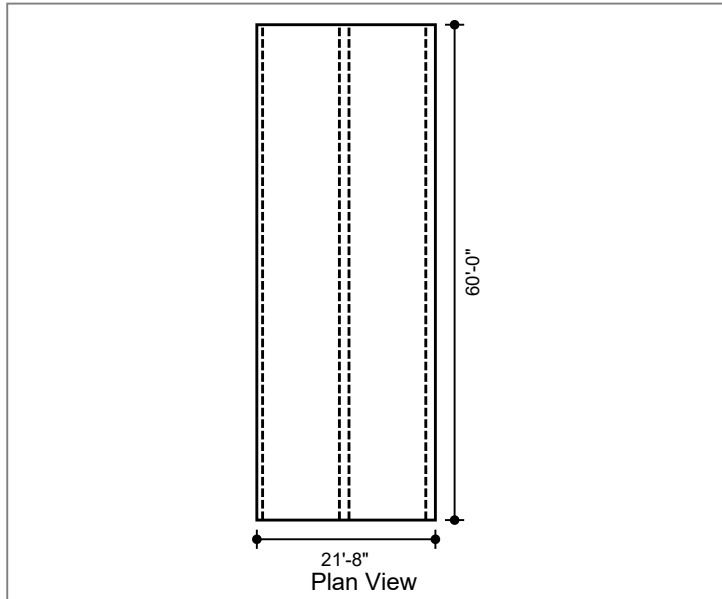
*Existing Culvert Analysis (Shored)*

---

Spec.: LRFD 9th ed.  
 Type of Culvert: Precast

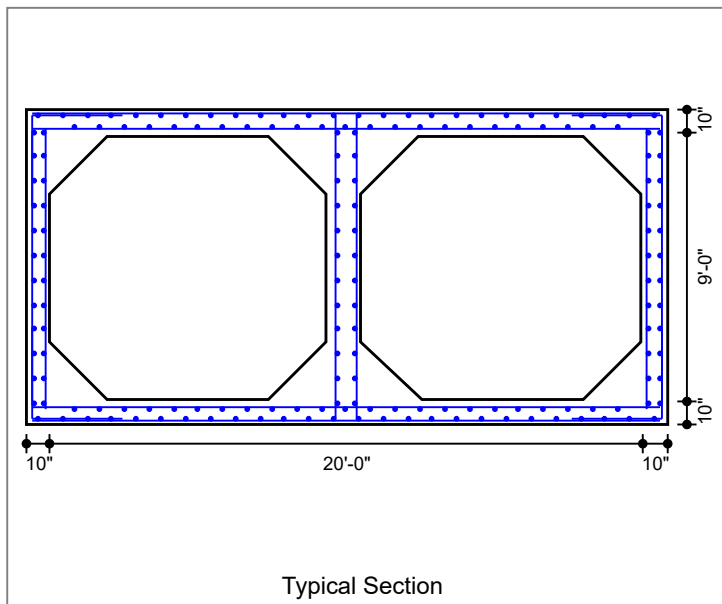
**Physical Dimensions**

Clear Span:	9'-6"
Clear Height:	9'-0"
Top Slab:	10"
Bottom Slab:	10"
Ext. Wall:	10"
Int. Wall:	1'-0"
Fill Depth Range	
Maximum:	6.00 ft
Minimum:	4.00 ft
Increment:	0.50 ft
Length:	60'-0"
Skew Angle:	0.00 deg
Bottom Slab Support:	Full Slab
Top Haunch, Width:	2'-0"
Top Haunch, Height:	2'-0"
Bottom Haunch, Width:	2'-0"
Bottom Haunch, Height:	2'-0"



**Material Properties**

<b>Concrete</b>	
Strength, f <sub>c</sub> :	5.000 ksi
Density:	0.155 kcf
Elasticity, E <sub>c</sub> :	4903 ksi
Type:	Normal wt
<b>Steel</b>	
Yield, f <sub>y</sub> :	60 ksi
Allow Stress:	36 ksi
Elasticity, E <sub>s</sub> :	29000 ksi
<b>Soil</b>	
Density:	0.127 kcf
Exposure Factor	
User-Defined:	1.00
<b>Reinforcement Covers</b>	
Ext. Cover Top Slab:	2"
Ext. Cover Bottom Slab:	2"
Ext. Cover Walls:	2"
Int. Cover Walls:	2"
Int. Cover Top Slab:	2"
Int. Cover Bottom Slab:	2"



**Controlling Ratings**

Inventory Rating: 1.26  
 Operating Rating: 1.63

**Loads**

<b>Live Load</b>			
Vehicle Names:	HL-93	EV 2	EV 3
	NRL - Legal Lane	NRL	Overload 1
	Overload 2	Type 3-3	Type 3
	Type 3S2	WA-105	
Traffic Direction:	Perpendicular		
Eq. Height of Soil:	Calculated		
Max No. of Lanes:	2		
<b>Dead Load</b>			
Future Wearing Surface:	0.000 klf	<b>Lateral Soil Loads</b>	
Additional Dead Load:	0.000 klf	Eq. Fluid Press. Max:	60.00 pcf
Concentrated Loads:	none	Eq. Fluid Press. Min:	30.00 pcf
Interior Water Pressure:	no		
Exterior Water Pressure:	no		

Project : Bothell to Swamp Creek  
 Task : Box Culvert Evaluation  
 Job No. :

Client: Skanska  
 File: Bothell DBC.etcx

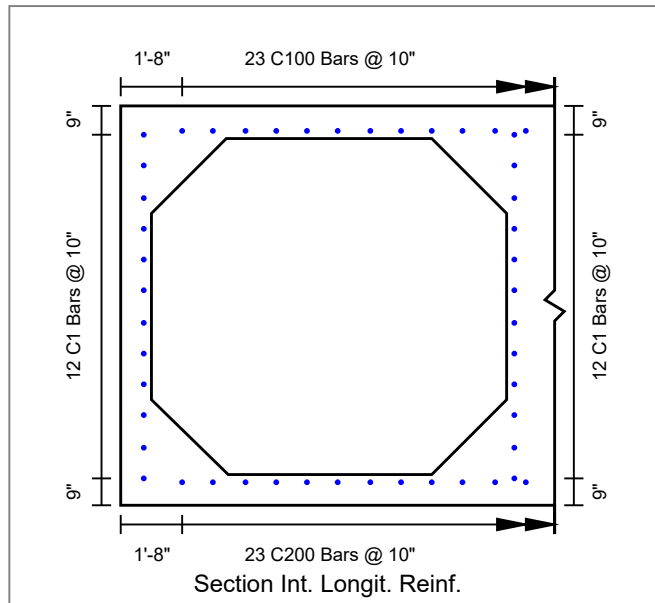
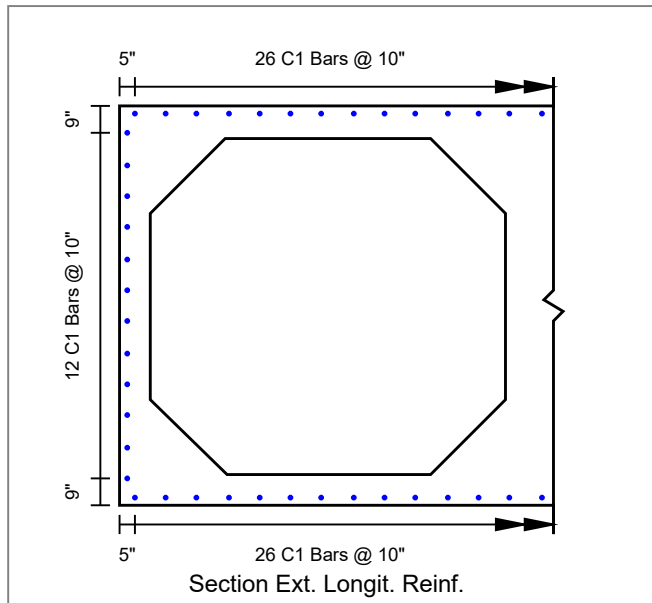
Sht \_\_\_\_\_ of \_\_\_\_\_  
 By: \_\_\_\_\_  
 Ck: \_\_\_\_\_  
 5/23/2025 5:27:51 PM  
 p. 2 of 4

**Concrete Summary**

Volume of Concrete: 2.819 cy/ft Total Volume of Concrete: 169.136 cy

**Reinforcing Steel Bar Schedule (lb)**

Location	Mark	Qty	Size	Spacing	Type	Length	Hor.Leg	Ver.Leg	Tot.Weight
Top Slab(Int)	A100 (AS2)	144	7	5"	S	21'-3"	--	--	6255.0
Bot Slab(Int)	A200 (AS3)	144	7	5"	S	21'-3"	--	--	6255.0
Top Slab(Ext)	A300 (AS7)	72	5	10"	S	21'-3"	--	--	1596.0
Bot Slab(Ext)	A400 (AS8)	72	5	10"	S	21'-3"	--	--	1596.0
Corner(Top)	A1 (AS1)	288	7	5"	L	6'-2"	3'-1"	3'-1"	3630.0
Corner(Bot)	A2 (AS1)	288	7	5"	L	6'-2"	3'-1"	3'-1"	3630.0
Wall(Int)	B1 (AS4)	288	5	5"	S	9'-6"	--	--	2854.0
Wall(Ext)	B2 (AS1)	288	7	5"	S	9'-0"	--	--	5298.0
Int Wall	B3	288	5	5"	S	10'-3"	--	--	3079.0
Longit. Top (Int)	C100 (AS5)	23	5	10"	S	59'-11"	--	--	1437.0
Longit. Bot (Int)	C200	23	5	10"	S	59'-11"	--	--	1437.0
Longit. Top (Ext)	C1 (AS6)	26	5	10"	S	59'-11"	--	--	1624.8
Longit. Bot (Ext)	C1 (AS6)	26	5	10"	S	59'-11"	--	--	1624.8
Longit. Wall (Ext)	C1 (AS6)	24	5	10"	S	59'-11"	--	--	1499.8
Longit. Wall (Int)	C1 (AS6)	24	5	10"	S	59'-11"	--	--	1499.8
Longit. Int	C1 (AS6)	24	5	10"	S	59'-11"	--	--	1374.8
									44691



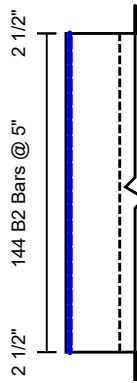
Project : Bothell to Swamp Creek

Task : Box Culvert Evaluation

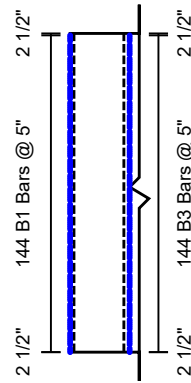
Job No. :

Client: Skanska

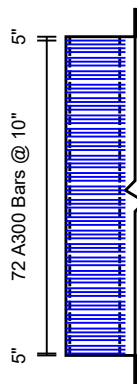
File: Bothell DBC.etcx



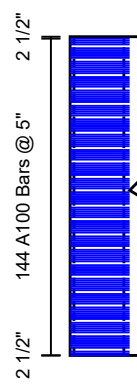
Ext. Wall Reinf.



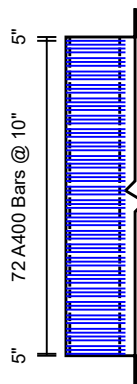
Int. Wall Reinf.



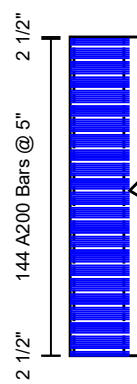
Top Slab Ext. Reinf.



Top Slab Int. Reinf.



Bottom Slab Ext. Reinf.



Bottom Slab Int. Reinf.

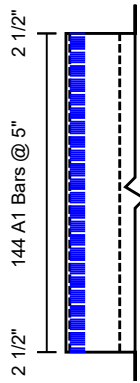
Project : Bothell to Swamp Creek

Task : Box Culvert Evaluation

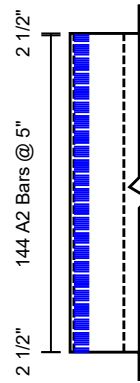
Job No. :

Client: Skanska

File: Bothell DBC.etcx



Top Slab Corner Reinf.



Bottom Slab Corner Reinf.

RATINGS SUMMARY  
 =====

Truck	Flexure			Shear		
	RF(INV)	RF(OP)	Controlling Point	RF(INV)	RF(OP)	Controlling Point
(AA) HL-93	1.45	1.88	Bottom Slab, RT	1.26	1.63	Bottom Slab, RT
(AB) EV 2	2.31	2.31	Bottom Slab, RT	2.04	2.04	Top Slab, RT
(AC) EV 3	2.49	2.49	Bottom Slab, RT	2.20	2.20	Top Slab, RT
(AD) NRL - Le	3.10	3.10	Bottom Slab, RT	2.73	2.73	Bottom Slab, RT
(AE) NRL	2.36	2.36	Bottom Slab, RT	2.08	2.08	Bottom Slab, RT
(AF) Oveload	3.86	3.86	Bottom Slab, RT	3.44	3.44	Top Slab, RT
(AG) Oveload	3.78	3.78	Bottom Slab, RT	3.36	3.36	Top Slab, RT
(AH) Type 3-3	2.51	2.51	Bottom Slab, RT	2.21	2.21	Bottom Slab, RT
(AI) Type 3	2.36	2.36	Bottom Slab, RT	2.08	2.08	Bottom Slab, RT
(AJ) Type 3S2	2.59	2.59	Bottom Slab, RT	2.28	2.28	Bottom Slab, RT
(AK) WA-105	2.36	2.36	Bottom Slab, RT	2.08	2.08	Bottom Slab, RT

REINFORCEMENT SUMMARY  
 =====

M dimension = 2' 5" (method of equivalent capacity)  
 = 6' 1" (method of contraflexure - ASTM)

Reinforcing steel Schedule  
 -----

Location	Bar Mark	Qty	Size	Type	Spacing (in)	As,prv (in <sup>2</sup> /ft)	Length (ft-in)	Wgt (lbs)	H Leg (ft-in)	V Leg (ft-in)
Top slab (int)	A100 (AS2)	144	7	STR	5.00	1.440	21- 3	6255		
Bot Slab (int)	A200 (AS3)	144	7	STR	5.00	1.440	21- 3	6255		
Top slab (ext)	A300 (AS7)	72	5	STR	10.00	0.372	21- 3	1596		
Bot Slab (ext)	A400 (AS8)	72	5	STR	10.00	0.372	21- 3	1596		
Corner (Top)	A1 (AS1)	288	7	L-BAR	5.00	1.440	6- 2	3630	3- 1	3- 1
Corner (Bottom)	A2 (AS1)	288	7	L-BAR	5.00	1.440	6- 2	3630	3- 1	3- 1
Ext wall (int)	B1 (AS4)	288	5	STR	5.00	0.744	9- 6	2854		
Ext wall (ext)	B2 (AS1)	288	7	STR	5.00	1.440	9- 0	5298		
Int wall	B3	288	5	STR	5.00	0.744	10- 3	3079		
Top slab (int- 1)	C100 (AS5)	23	5	STR	10.00	0.372	59-11	1437		
Bot Slab (int- 1)	C200	23	5	STR	10.00	0.372	59-11	1437		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1375		
Total								44691		

Note: A denotes flexural steel, B denotes vertical steel, C denotes longitudinal steel

AS Bar Marks  
 -----

Location	As prv in <sup>2</sup> /ft
Transverse Side wall - Outside Face (AS1)	1.440
Transverse Top Slab - Inside Face (AS2)	1.440
Transverse Bottom Slab - Inside Face (AS3)	1.440
Transverse Side wall - Inside Face (AS4)	0.744
Distribution Top Slab - Inside Face (AS5)	0.372
Distribution Top Slab - Outside Face (AS6)	0.372
Transverse Top Slab - Outside Face (AS7)	0.372
Transverse Bottom Slab - Outside Face (AS8)	0.372

Notes: 1.) Final areas of steel provided must be checked in analysis mode

Project: Bothell to Swamp Creek  
 Task : Box Culvert Evaluation  
 Client : Skanska  
 Job No.:

CULVERT PROPERTIES

=====  
 Type of Culvert: Precast Specification : LRFD 9th Edition  
 Operating Mode : Analysis

Physical Dimensions

-----  
 No. of Boxes: 2 Name: BoxCulvert  
 Clear Span : 9.5000 ft  
 Clear Height: 9.0000 ft Skew Angle : 0.00 deg  
 Length : 60.0000 ft Bottom Slab Support: Full Slab  
 Fill Depth Range: Maximum : 6.00 ft Minimum : 4.00 ft Increment : 0.50 ft  
 Haunches: Top, Length: 24.0000 in Height: 24.0000 in  
 Bottom, Length: 24.0000 in Height: 24.0000 in  
 Member Thicknesses: Top Slab: 10.0000 in Bot Slab: 10.0000 in  
 Ext wall: 10.0000 in Int wall: 12.0000 in  
 Wall Joint: None

Material Properties

-----  
 Concrete: Strength, f'c : 5.000 ksi Density : 0.155 kcf Elasticity, Ec: 4903 ksi  
 Type : Normal weight Density Modification Factor : 1.00  
 Fr Factor : 0.24 Gamma1 : 1.60 Gamma3 : 1.00 (user defined)  
 Steel: Yield, fy : 60.00 ksi fss Limit : 0.60fy Elasticity, Es: 29000 ksi  
 Yield, fyv : 60.00 ksi Diameter : 1.000 in Type : Rebar  
 Soil: Density : 0.127 kcf Slope Factor: 1.150  
 Poisson's : 0.5  
 Fe Factor : 1.000 (User Defined)  
 Serviceability, Gamma-e: 1.00

Loads

-----  
 Live Load: Vehicle: (AA) HL-93 - Design Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 8.00 0.00  
 2 32.00 14.00  
 3 32.00 14.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: yes  
 Tandem: Axle 1: 25.00 k, Axle 2: 25.00 k, Axle Spacing: 4.00 ft  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Inventory Rating Load Factor: 1.75 Operating Rating Load Factor: 1.35  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no  
 Vehicle: (AB) EV 2 - Permit Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 24.00 0.00  
 2 33.50 15.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck Or Tandem Or Lane  
 Rating Load Factor: 1.3  
 Design Load Combinations: Strength II  
 Override MPF: no  
 Override DLA: no  
 Vehicle: (AC) EV 3 - Permit Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 24.00 0.00  
 2 31.00 15.00  
 3 31.00 4.00  
 Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in  
 Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck Or Tandem Or Lane  
 Rating Load Factor: 1.3  
 Design Load Combinations: Strength II  
 Override MPF: no  
 Override DLA: no  
 Vehicle: (AD) NRL - Legal Lane - Legal Vehicle  
 Axle No. weight(k) Dist. From Previous(ft)  
 1 10.50 0.00  
 2 10.50 4.00

3	12.00	16.00
4	9.00	15.00
5	9.00	4.00
6	9.00	15.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
Lane Load: 0.20 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 2  
Design Load Combinations: Strength I

Override MPF: no  
Override DLA: no

Vehicle: (AE) NRL - Legal Vehicle

Axle No.	weight(k)	Dist. From Previous(ft)
1	8.00	0.00
2	8.00	4.00
3	8.00	4.00
4	17.00	4.00
5	17.00	4.00
6	8.00	4.00
7	8.00	4.00
8	6.00	6.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 2  
Design Load Combinations: Strength I

Override MPF: no  
Override DLA: no

Vehicle: (AF) Oveload 1 - Permit Vehicle

Axle No.	weight(k)	Dist. From Previous(ft)
1	21.50	0.00
2	21.50	4.00
3	21.50	12.00
4	21.50	4.00
5	10.00	10.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 1.2  
Design Load Combinations: Strength II

Override MPF: no  
Override DLA: no

Vehicle: (AG) Oveload 2 - Permit Vehicle

Axle No.	weight(k)	Dist. From Previous(ft)
1	22.00	0.00
2	21.50	6.00
3	21.50	4.00
4	22.00	14.00
5	21.50	6.00
6	21.50	4.00
7	22.00	16.00
8	21.50	6.00
9	21.50	4.00
10	12.00	10.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 1.2  
Design Load Combinations: Strength II

Override MPF: no  
Override DLA: no

Vehicle: (AH) Type 3-3 - Legal Vehicle

Axle No.	weight(k)	Dist. From Previous(ft)
1	14.00	0.00
2	14.00	4.00
3	16.00	16.00
4	12.00	15.00
5	12.00	4.00
6	12.00	15.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
Combine: Truck + Lane Or Tandem + Lane  
Rating Load Factor: 2  
Design Load Combinations: Strength I

Override MPF: no  
Override DLA: no

Vehicle: (AI) Type 3 - Legal Vehicle

Axle No.	Weight(k)	Dist. From Previous(ft)
1	17.00	0.00
2	17.00	4.00
3	16.00	15.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no

Vehicle: (AJ) Type 3S2 - Legal Vehicle

Axle No.	Weight(k)	Dist. From Previous(ft)
1	15.50	0.00
2	15.50	4.00
3	15.50	22.00
4	15.50	4.00
5	10.00	11.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no

Vehicle: (AK) WA-105 - Legal Vehicle

Axle No.	Weight(k)	Dist. From Previous(ft)
1	14.00	0.00
2	14.00	4.00
3	17.00	10.00
4	17.00	32.00
5	17.00	4.00
6	7.00	4.00
7	7.00	4.00
8	12.50	11.00

Gage width: 6.00 ft, Tread width: 20.00 in, Tread Length: 10.00 in

Include Tandem: no  
 Lane Load: 0.00 klf, P-Moment: 0.00 k, P-Shear: 0.00 k  
 Combine: Truck + Lane Or Tandem + Lane  
 Rating Load Factor: 2  
 Design Load Combinations: Strength I  
 Override MPF: no  
 Override DLA: no

Include Lane Load : yes Max. No. of Lanes: 2  
 Traffic Direction : Lanes Perpendicular to Main Reinforcement  
 Neglect Live Load if: Fill > 8 ft and Fill > Clear Span  
 Apply Surcharge at Fill Depths > 2 ft : yes  
 Compute Surcharge Depth: yes

Dead Load: Future wearing Surface : 0.00 klf Add. Dead Load : 0.00 klf  
 Concentrated Loads : none

Lateral Soil Loads: Max. Equiv. Fluid Press.: 60.00 pcf Min. Equiv. Fluid Press. : 30.00 pcf

Include Additional Uniform Horiz. Load: no  
 Include Additional Uniform Vert. Load: no  
 Buoyancy Check : no  
 Fluid Pressures : Apply Water Press. : no  
 Foundation Model : Uniform Loads  
 Seismic Analysis : Do not include

Load and Resistance Factors

DC:	1.250	Max	0.900	Min			
DW:	1.500	0.650					
EV:	1.300	0.900					
EH:	1.350	0.900					
WA:	1.000						
EQ:	1.000						
LL I	: 1.750	LL II	: 1.350	LL Legal	: 1.750	LL Extreme	: 0.500
Ductility:	1.000	Importance:	1.000	Redundancy, non-earth:	1.000	Redundancy, earth:	1.000
Condition:	1.000	System	: 1.000				
Phi Shear:	0.900	Phi Moment:	1.000	PM Compression:	0.750	PM Tension	: 0.900
Load Factor Multipliers, Design Mode:	1.00	Analysis Mode:	1.00				

Reinforcement

Reinforcement Covers :	Exterior	Interior
Top Slab:	2.0000 in	2.0000 in
walls :	2.0000 in	2.0000 in
Bot Slab:	2.0000 in	2.0000 in

Assigned reinforcement:

Location	Mark	Size	Spacing (in)
Top Slab Inside	A100 (AS2)	7	5.0000
Bottom Slab Inside	A200 (AS3)	7	5.0000
Top Slab Outside	A300 (AS7)	5	10.0000
Bottom Slab Outside	A400 (AS8)	5	10.0000
Top Corner	A1 (AS1)	7	5.0000
Bottom Corner	A2 (AS1)	7	5.0000
Ext. Wall Inside	B1 (AS4)	5	5.0000
Ext. wall Outside	B2 (AS1)	7	5.0000
Interior wall	B3	5	5.0000
Longitudinal	C1 (AS6)	5	10.0000
Top Distribution	C100 (AS5)	5	10.0000
Bottom Distribution	C200	5	10.0000

Analysis Options

-----

LL Analysis : Automatically Set Traffic Direction to Account for Skew Effects: no  
 Limit LL Distribution width to Culvert Length for: None  
 Combine Longitudinal Axle Distribution Overlaps: No  
 Combine Transverse Axle Distribution Overlaps: No  
 Axle Placement Increment for Moving Load Analysis: 20  
 Include Impact on Bottom Slab: yes  
 Always distribute wheel Load: yes  
 Deflection Criteria : 1/800  
 Approach Slab will be Used: no

Reinforcement : Always Include Distribution Steel: no  
 Distribution Slab Provided: no  
 User Defined Longitudinal Steel: yes  
 Max. As used in Vc Calcs: 2.00 in<sup>2</sup>/ft  
 Distribute Minimum Reinforcement per Face: yes  
 Use individual Member Thicknesses for Min Steel: no  
 Epoxy coat steel: no  
 Use M-dimension for bar length calcs.: no

Slenderness : Checked K Factor: 2.00

Analysis Modeling : Use Haunches in the Structural Analysis Model: yes

Critical Sections : Flexure critical section location: 1.5 member depth  
 Shear critical section location: dv beyond support  
 Use Max. Moment with Max. Shear at the Critical Section for Shear: no  
 Include depth of haunch for critical sections: no

Flexure : Ignore Axial Thrust: no  
 Use Eq. 12.10.4.2.4a-1: yes Nu Multiplier: 1.00

Shear : Always Check Iterative Beta Method

Environmental : Apply durability factors: no

Load Combinations : LRFD min/min: no

ANALYSIS RESULTS  
 =====

Top Slab Thickness = 10.00 in  
 Bottom Slab Thickness = 10.00 in  
 Exterior Wall Thickness = 10.00 in  
 Interior Wall Thickness = 12.00 in

Modular Ratio (N) = 5.91 Max. Steel Ratio = 0.025  
 Design Span = 10.42 ft Design Height = 9.83 ft

Volume of Concrete: 2.819 cy/ft weight of Steel: 745 lb/ft

Note: Design and analysis results do not include force effects from stipping and handling stages

M dimension = 2' 5" (method of equivalent capacity)  
 = 6' 1" (method of contraflexure - ASTM)

Reinforcing Steel Schedule  
 -----

Location	Bar Mark	Qty	Size	Type	Spacing (in)	As,prv (in <sup>2</sup> /ft)	Length (ft-in)	Wgt (lbs)	H Leg (ft-in)	V Leg (ft-in)
Top Slab (int)	A100 (AS2)	144	7	STR	5.00	1.440	21- 3	6255		
Bot Slab (int)	A200 (AS3)	144	7	STR	5.00	1.440	21- 3	6255		
Top Slab (ext)	A300 (AS7)	72	5	STR	10.00	0.372	21- 3	1596		
Bot Slab (ext)	A400 (AS8)	72	5	STR	10.00	0.372	21- 3	1596		
Corner (Top)	A1 (AS1)	288	7	L-BAR	5.00	1.440	6- 2	3630	3- 1	3- 1
Corner (Bottom)	A2 (AS1)	288	7	L-BAR	5.00	1.440	6- 2	3630	3- 1	3- 1
Ext wall (int)	B1 (AS4)	288	5	STR	5.00	0.744	9- 6	2854		
Ext wall (ext)	B2 (AS1)	288	7	STR	5.00	1.440	9- 0	5298		
Int wall	B3	288	5	STR	5.00	0.744	10- 3	3079		
Top Slab (int- 1)	C100 (AS5)	23	5	STR	10.00	0.372	59-11	1437		
Bot Slab (int- 1)	C200	23	5	STR	10.00	0.372	59-11	1437		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	26	5	STR	10.00	0.372	59-11	1625		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1500		
Temperature ( 1)	C1 (AS6)	24	5	STR	10.00	0.372	59-11	1375		
Total								44691		

Note: A denotes flexural steel, B denotes vertical steel, C denotes longitudinal steel

AS Bar Marks  
 -----

Location	As prv in <sup>2</sup> /ft
Transverse Side Wall - Outside Face (AS1)	1.440
Transverse Top Slab - Inside Face (AS2)	1.440
Transverse Bottom Slab - Inside Face (AS3)	1.440
Transverse Side Wall - Inside Face (AS4)	0.744
Distribution Top Slab - Inside Face (AS5)	0.372
Distribution Top Slab - Outside Face (AS6)	0.372
Transverse Top Slab - Outside Face (AS7)	0.372
Transverse Bottom Slab - Outside Face (AS8)	0.372

Notes: 1.) Final areas of steel provided must be checked in analysis mode

Summary of Ratings Table:  
 -----

Truck	Flexure							Shear				
	ILF	OLF	Fill	Member	Location	IR	OR	Fill	Member	Location	IR	OR
(AA)HL-93	1.75	1.35	4.00	4	RT	1.45	1.88	4.00	4	RT	1.26	1.63
(AB)EV 2	1.30	1.30	4.00	4	RT	2.31	2.31	4.00	2	RT	2.04	2.04
(AC)EV 3	1.30	1.30	4.00	4	RT	2.49	2.49	4.00	2	RT	2.20	2.20
(AD)NRL -	2.00	2.00	4.00	4	RT	3.10	3.10	4.00	4	RT	2.73	2.73
(AE)NRL	2.00	2.00	4.00	4	RT	2.36	2.36	4.00	4	RT	2.08	2.08
(AF)Oveloa	1.20	1.20	4.00	4	RT	3.86	3.86	4.00	2	RT	3.44	3.44
(AG)Oveloa	1.20	1.20	4.00	4	RT	3.78	3.78	4.00	2	RT	3.36	3.36
(AH)Type 3	2.00	2.00	4.00	4	RT	2.51	2.51	4.00	4	RT	2.21	2.21
(AI)Type 3	2.00	2.00	4.00	4	RT	2.36	2.36	4.00	4	RT	2.08	2.08
(AJ)Type 3	2.00	2.00	4.00	4	RT	2.59	2.59	4.00	4	RT	2.28	2.28
(AK)WA-105	2.00	2.00	4.00	4	RT	2.36	2.36	4.00	4	RT	2.08	2.08

Critical Sections Summary: Flexure  
 -----

Member 1: (Exterior wall), Thickness = 10.00 in  
 Design Corr.

Loc	Dist. (in)	Moment (k-ft)	A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)	phi	As (in2)	Mcr (k-ft)	IR	OR	Truck	Depth (ft)
BOT	24.00	-5.65	10.35	48.35	7.56	51.12	1.00	1.44	14.31	18.53	24.02	AA	4.00
MID	59.00	2.50	3.71	26.97	7.69	28.23	1.00	0.74	14.31	19.94	25.85	AA	4.00
MID-	59.00	-4.32	9.55	48.35	7.56	50.91	1.00	1.44	14.31	15.25	19.77	AA	4.00
TOP	24.00	-7.28	10.35	48.35	7.56	51.12	1.00	1.44	14.31	10.26	13.30	AA	4.00

Member 2: (Top Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Moment (k-ft)	Corr. A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)	phi	As (in2)	Mcr (k-ft)	Load Ratings		Truck	Fill Depth (ft)
										IR	OR		
LT	24.00	-3.20	5.20	48.35	7.56	49.76	1.00	1.44	14.31	36.28	47.03	AA	6.00
MID	50.00	8.90	0.75	48.35	7.56	48.56	1.00	1.44	14.31	7.72	10.00	AA	4.00
MID-	50.00	0.40	4.86	13.89	7.69	15.72	1.00	0.37	14.31	NC	NC	AA	6.00
RT	25.00	-10.13	1.90	13.66	7.56	14.38	1.00	0.37	14.31	1.72	2.23	AA	4.00

Member 3: (Interior wall), Thickness = 12.00 in

Loc	Dist. (in)	Design Moment (k-ft)	Corr. A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)	phi	As (in2)	Mcr (k-ft)	Load Ratings		Truck	Fill Depth (ft)
										IR	OR		
BOT	23.00	-2.33	23.26	34.41	9.69	43.90	1.00	0.74	20.61	NC	NC	AA	4.50
MID	59.00	3.04	11.48	34.41	9.69	39.20	1.00	0.74	20.61	12.88	16.69	AA	4.00
TOP	23.00	-6.35	24.55	34.41	9.69	44.40	1.00	0.74	20.61	6.99	9.06	AA	4.00

Member 4: (Bottom Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Moment (k-ft)	Corr. A. F. (k)	Mu (k-ft)	ds (in)	Ma (k-ft)	phi	As (in2)	Mcr (k-ft)	Load Ratings		Truck	Fill Depth (ft)
										IR	OR		
LT	24.00	-3.60	6.96	48.35	7.56	50.23	1.00	1.44	14.31	37.19	48.21	AA	6.00
MID	50.00	8.05	1.82	48.35	7.56	48.85	1.00	1.44	14.31	10.76	13.95	AA	4.00
MID-	50.00	0.55	6.58	13.89	7.69	16.36	1.00	0.37	14.31	NC	NC	AA	6.00
RT	25.00	-12.01	2.96	13.66	7.56	14.78	1.00	0.37	14.31	1.45	1.88	AA	4.00

Critical Sections Summary: Vertical Shear

Member 1: (Exterior wall), Thickness = 10.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in2)	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
BOT	12.20	5.42	9.7	9.61	7.20	18.77	3.416	20.85 a	0.00	0.00	0.00	11.34	14.70	AA	6.00
MID	59.00	0.62	2.5	3.71	7.25	23.36	4.223	25.96 a	0.00	0.00	0.00	41.25	53.48	AA	4.00
MID-	59.00	0.66	4.3	9.55	7.20	25.17	4.581	27.97 a	0.00	0.00	0.00	41.98	54.41	AA	4.00
TOP	12.20	-4.38	10.4	9.61	7.20	18.64	3.393	20.71 a	0.00	0.00	0.00	11.26	14.59	AA	6.00

Member 2: (Top Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in2)	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
LT	12.20	7.98	6.7	4.70	7.56	19.92	3.451	22.13 a	0.00	0.00	0.00	3.51	4.55	AA	4.00
MID	62.50	0.33	7.6	0.75	7.56	20.87	3.616	23.19 a	0.00	0.00	0.00	38.12	49.41	AA	4.00
MID-	62.50	2.72	0.6	4.70	7.69	21.88	3.730	24.32 a	0.00	0.00	0.00	11.39	14.76	AA	4.00
RT	13.20	11.06	19.5	1.90	7.56	12.89	n/a	14.33 c	0.00	0.00	0.00	1.28	1.66	AA	4.00

Member 3: (Interior wall), Thickness = 12.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in2)	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
BOT	13.64	1.10	1.2	22.94	9.25	35.60	5.043	39.56 a	0.00	0.00	0.00	32.29	41.86	AA	4.00
MID	59.00	1.10	3.0	11.48	9.25	34.86	4.939	38.74 a	0.00	0.00	0.00	31.63	41.00	AA	4.00
TOP	13.64	1.10	7.2	24.55	9.25	34.97	4.953	38.85 a	0.00	0.00	0.00	31.72	41.12	AA	4.00

Member 4: (Bottom Slab), Thickness = 10.00 in

Loc	Dist. (in)	Design Shear (k)	Corr. Moment (k-ft)	Corr. A. F. (k)	Dv (in)	phi*Vn	Beta	Vc (k)	Vs (k)	Av (in2)	Max. Spac (in)	Load Ratings		Truck	Fill Depth (ft)
												IR	OR		
LT	12.20	7.46	7.7	6.96	7.56	19.90	3.448	22.11 a	0.00	0.00	0.00	7.15	9.27	AA	6.00
MID	62.50	0.24	6.6	1.82	7.56	21.78	3.774	24.20 a	0.00	0.00	0.00	60.23	78.08	AA	4.00
MID-	62.50	2.56	0.0	5.89	7.69	23.39	4.042	25.99 a	0.00	0.00	0.00	64.83	84.04	AA	4.00
RT	13.20	11.42	22.3	2.96	7.56	12.84	n/a	14.27 c	0.00	0.00	0.00	1.26	1.63	AA	4.00

Vc Calculation By: a - Iterative Beta, b - Constant Beta, c - Box Culvert, d - Standard/Arema

---

## *Culvert Shoring Calculations*

---

Unfactored Thrusts due to All Loads: (k) (Fill Depth = 4.00 ft)

Member	Pdc	Pev	Pdw	Peh	Pls	Pwa
1	0.79	1.92	0.00	0.69	0.19	0.00
2	-0.18	0.02	0.00	2.22	0.74	0.00
3	2.92	6.74	0.00	-1.37	-0.39	0.00
4	0.18	-0.02	0.00	3.28	0.75	0.00

Analysis Truck, HL-93

HL-93 load  
 distribution on box  
 culvert

Vehicle	Axle No.	Weight (k/ft)	Length (ft)	Dist. From Previous (ft)
Truck	1	0.495	6.27	
	2	0.495	6.27	6.00
	3	0.495	6.27	4.00
	4	0.495	6.27	6.00
Tandem	1	0.387	6.27	
	2	0.387	6.27	6.00
	3	0.387	6.27	4.00
	4	0.387	6.27	6.00

Live Load Parameters:

Traffic Direction is Perpendicular to Main Reinforcement  
 Distribution Width : 6.00 ft  
 Impact Factor : 1.17  
 Truck MPF : 1.20 Tandem MPF : 1.20  
 Lane Load Distribution Width : 15.17 ft  
 Lane Load: 0.000 k/ft

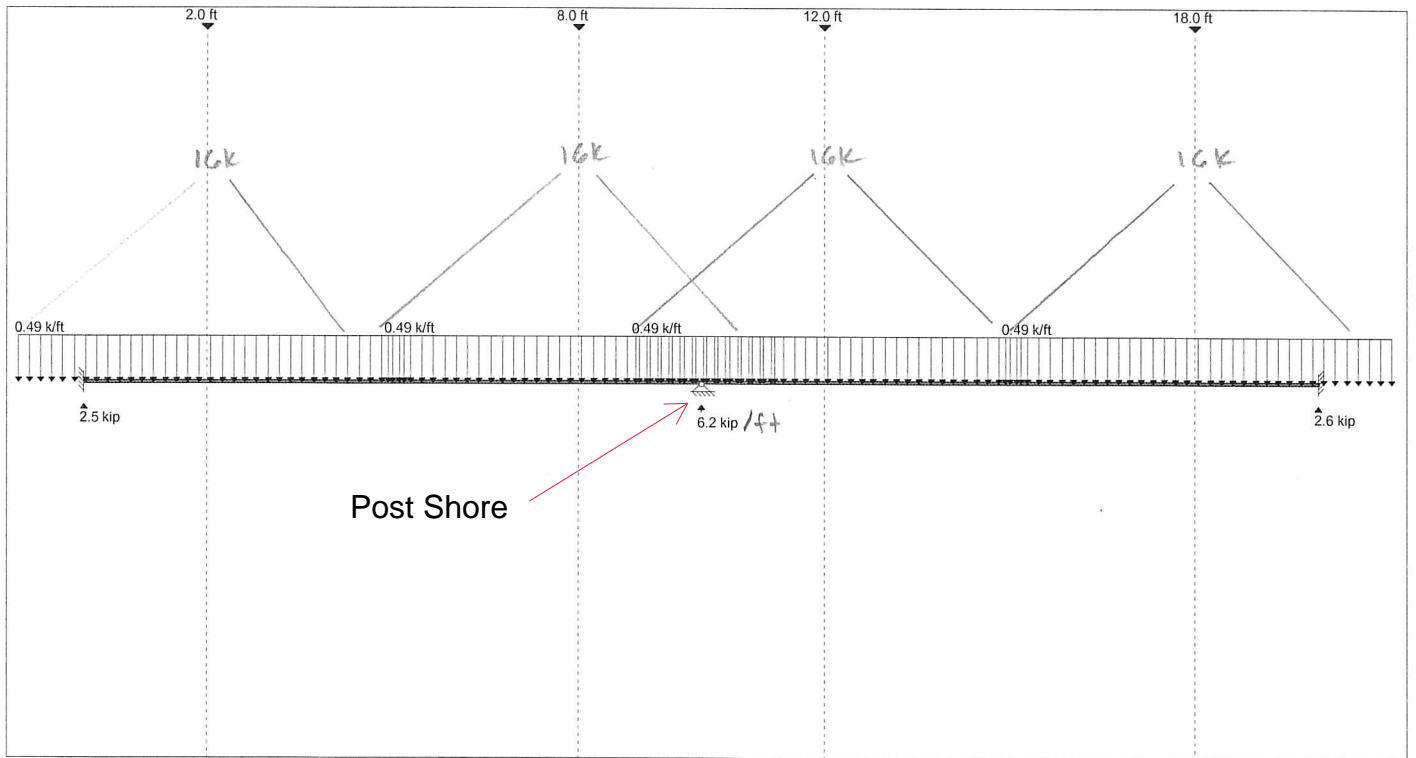
Truck Positions That Cause Maximum Results:

Maximum +Moment in Top Slab					Maximum -Moment in Top Slab				
Vehicle	Axle No.	Weight (klf)	Length (ft)	Dist. From Left End (ft)	Vehicle	Axle No.	Weight (klf)	Length (ft)	Dist. From Left End (ft)
Truck	1	0.495	6.27	11.97	Truck	1	0.495	6.27	14.95
	2	0.495	6.27	5.97		2	0.495	6.27	8.95
	3	0.495	6.27	1.97		3	0.495	6.27	4.95
	4	0.495	6.27	-4.03		4	0.495	6.27	-1.05
Maximum +Moment : 3.37 k-ft					Maximum -Moment : -10.73 k-ft				
Corresponding Moment at End : -3.02 k-ft					Corresponding Moment at Mid : 2.30 k-ft				
Coincident Bottom Slab Load : 0.42 k/ft					Coincident Bottom Slab Load : 0.50 k/ft				
Maximum +Shear in Top Slab					Maximum -Shear in Top Slab				
Truck	1	0.495	6.27	9.13	Truck	1	0.495	6.27	17.28
	2	0.495	6.27	3.13		2	0.495	6.27	11.28
	3	0.495	6.27	-0.87		3	0.495	6.27	7.28
	4	0.495	6.27	-6.87		4	0.495	6.27	1.28
Maximum +Shear : 3.20 k					Maximum -Shear : -4.43 k				
Corresponding Shear at Mid : -0.50 k					Corresponding Shear at Mid : -0.72 k				
Coincident Bottom Slab Load : 0.35 k/ft					Coincident Bottom Slab Load : 0.55 k/ft				
Maximum +Moment in Top Slab					Maximum -Moment in Top Slab				
Tandem	1	0.387	6.27	11.97	Tandem	1	0.387	6.27	14.95
	2	0.387	6.27	5.97		2	0.387	6.27	8.95
	3	0.387	6.27	1.97		3	0.387	6.27	4.95
	4	0.387	6.27	-4.03		4	0.387	6.27	-1.05
Maximum +Moment : 2.64 k-ft					Maximum -Moment : -8.39 k-ft				
Corresponding Moment at End : -2.36 k-ft					Corresponding Moment at Mid : 1.79 k-ft				
Coincident Bottom Slab Load : 0.33 k/ft					Coincident Bottom Slab Load : 0.39 k/ft				
Maximum +Shear in Top Slab					Maximum -Shear in Top Slab				
Tandem	1	0.387	6.27	9.13	Tandem	1	0.387	6.27	17.28
	2	0.387	6.27	3.13		2	0.387	6.27	11.28
	3	0.387	6.27	-0.87		3	0.387	6.27	7.28
	4	0.387	6.27	-6.87		4	0.387	6.27	1.28
Maximum +Shear : 2.50 k					Maximum -Shear : -3.46 k				
Corresponding Shear at Mid : -0.39 k					Corresponding Shear at Mid : -0.56 k				
Coincident Bottom Slab Load : 0.27 k/ft					Coincident Bottom Slab Load : 0.43 k/ft				

Unfactored Moments and Shears due to Truck Loads: (k-ft, k)

M-PT	Truck				Tandem				Lane			
	M11+	M11-	V11+	V11-	M11+	M11-	V11+	V11-	M11+	M11-	V11+	V11-
Member 1: (Exterior wall)												

### HL-93 Wheel Load on Box Culvert



Beam Parameters: Length = 20.0 ft, [REDACTED]

Shore capacity = 8.5 kips

Shore max spacing =  $8.5/6.2 = 1.37' = 16''$

**Check Punching Shear at Slab**

f'c	5000	psi	
d	7.69	in	
Load Factor, LF	1.0		Max LF for LL
Load, P	8.5	kips	Load per shore
c1	5	in	Dimensions of Jack Base Bracket
c2	5	in	
$b_0 = 2(c1+d)+2(c2+d)$	50.75	in	Critical Shear perimeter
$\phi$	0.75		
$V_u = P * LF$	9	kips	
$\phi V_c = \phi(4 * f'c^{0.5} * b_0 * d)$	83	kips	OK ACI Eq 11-33

**Check Shear at Slab**

$\phi$	0.75		
b	12	in	
d	7.69	in	
f'c	5000	psi	
$\phi V_c = \phi(2 * f'c^{0.5} * b * d)$	9785	lbs per ft	
$V_u = w l / 2$	7215	lbs	OK

**Check Longitudinal Slab Bending Between Shoring Posts**

f'c	5000	psi	
f <sub>y</sub>	60000	psi	
b	12	in	
No. Bar	5		
db	0.625	in	
As per bar	0.31	in <sup>2</sup> /bar	
Spacing	10	in	
As per width "b"	0.37	in <sup>2</sup> /ft	
Slab Thickness, t	10	in	
$d = t - 2" \text{ cover} - 0.5 * db$	7.69	in	
$a = A_s * f_y / (0.85 * f'c * b)$	0.44	in	
$\phi$	0.9		
$\phi M_n = \phi A_s * f_y * (d - a / 2)$	12503	lb-ft /ft	
w (Strength I, factored)	10850	plf	
Span, l	1.33	ft	
$M = w l^2 / 8$	2399.1	lb-ft	OK

# The best possible "support" on your site – Doka floor props



- Doka floor props always have the same safe working load at any extension eliminating field calculation
- Doka floor props are light weight
- Doka floor props are galvanized – no rust
- Doka floor props come with accessories for both H20 and Alu beams

The numbered holes are a convenient feature that makes for quicker and easier height adjustments.

## Eurex 30

**8.5**  
kips  
(\*)

(\*) over entire extension range



Eurex 30 floor props						
Type	Article Number	closed	extended	weight	Safe working load	safety factor
Eurex 30 250	586092000	5' - 0"	8' - 2"	33 lbs	8,5 kips (37,8 kN) (**)	3 : 1
Eurex 30 300	586093000	5' - 8"	9' - 10"	37 lbs		3 : 1
Eurex 30 350	586094000	6' - 6"	11' - 5"	45 lbs		3 : 1
Eurex 30 400	586095000	7' - 6"	13' - 1"	55 lbs		3 : 1

(\*\*) according to DOKA TEST REPORT on compressions test for Doka-post-shores EUREX 30 8.5 kips. Nr. 861/01, Date: 27.09.2001 and US-Standards

**doka**  
The Formwork Experts

Osterreichische Doka  
Schalungstechnik GmbH  
Reichsstrasse 23  
A-3200 Amstetten / Austria  
Tel. +43 7472 505-0  
Fax +43 7472 605 54430  
E-Mail: Oest.Doka@doka.com

Northeast Office  
Corporate Headquarters:  
Conesco Industries, Ltd.  
214 Gates Road  
Little Ferry, NJ 07642  
Tel. 201-641-6500  
Fax 201-641-6254

Florida Office  
Conesco Industries, Ltd.  
838 Midham St.  
Banco De Desaro  
LLO Economico Bldg  
Suite 110-79  
San Juan, PR 00929  
Tel 787-277-3560  
Fax 787-783 9011

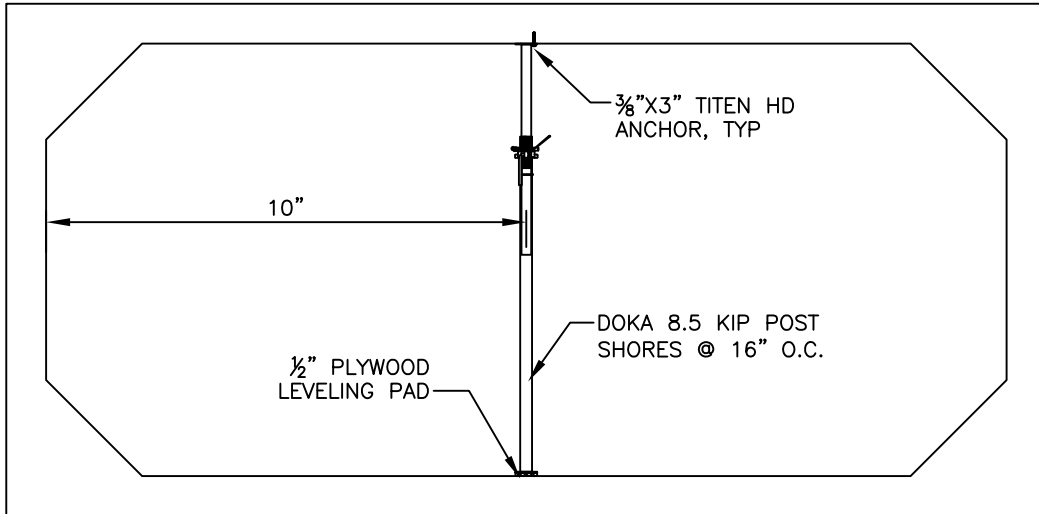
Texas Office:  
Conesco Industries, Ltd.  
1840 Halvey Way  
Suite 204 & 208  
Carrington, TX 75607  
Tel 972-446-1662/1663  
Fax 972-446-1772

Mid-Atlantic Office:  
Conesco Industries, Ltd.  
6637 Mid Cities Avenue  
Beltsville, MD 20705  
Tel 301-295-1900  
Fax 301-566-7305

Southeast Office  
Conesco Industries, Ltd.  
195A Boulderbrook Circle  
Lawrenceville, GA 30045  
Tel 770-962-7914  
Tel 888-636-4700  
Fax 770-962-9228

Midwest Office:  
Conesco Industries, Ltd.  
1032 Mason Avenue  
Rockdale, IL 60430  
Tel 815-730-8700  
Fax 815-730-4770

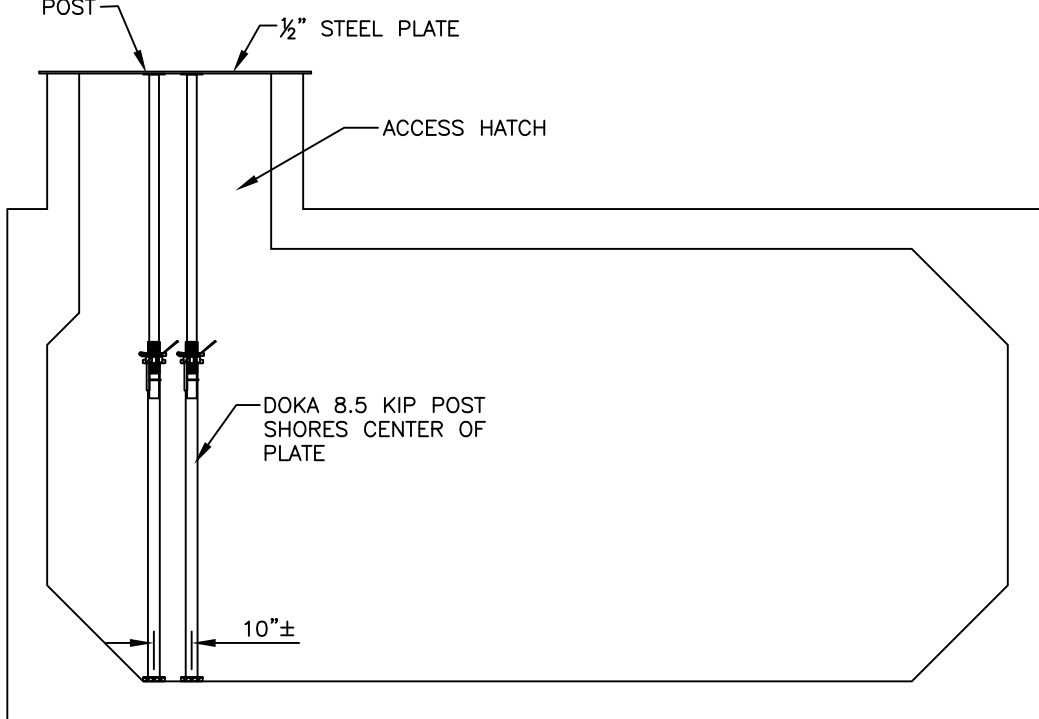
Internet: <http://www.doka.com>



BOX CULVERT TEMP SHORING

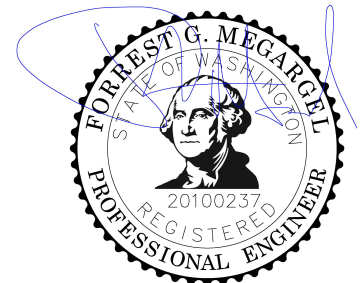
SCALE: 1:4

1EA.  $\frac{3}{8}$ "X1" SELF TAPPING BOLT IN PREDRILLED HOLES PER POST



HATCH LID TEMP SHORING

SCALE: 1:4



6-3-25

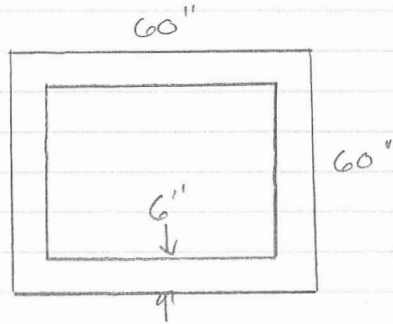
---

## *Access Riser Calculations*

---



## Concrete Riser



$$\text{Area} = 108 \text{ in}^2$$

Assume min steel = 12 no. 3's

$$\begin{aligned} \text{Riser Load} &= \text{HL-93 wheel load} + \text{Soil DL} \\ &= 1.75 (16,000) + 1.75 (2' \cdot 127) (5^2) = 35,938 \text{ lbs} \end{aligned}$$

$$\text{Compressive stress} = \frac{35,938 \text{ lbs}}{108 \text{ in}^2} = 333 \text{ psi}$$

**Check Concrete Risers as Concrete Columns**

Dead Load	6.35	kips	
Live Load	16.0	kips	
Design Load (Vertical)	36	kips	1.25 DL + 1.75LL

Lateral Load	0	kips	
Divided over 4 supports (Lateral)	0	kips	

$f'_c$	3.5	ksi	
$f_y$	60	ksi	
$\rho_{trial}$	0.03		
$A_{g\_trial}$	17.0	sq in	
	4.1	in	

**Check w/ #3 bars**

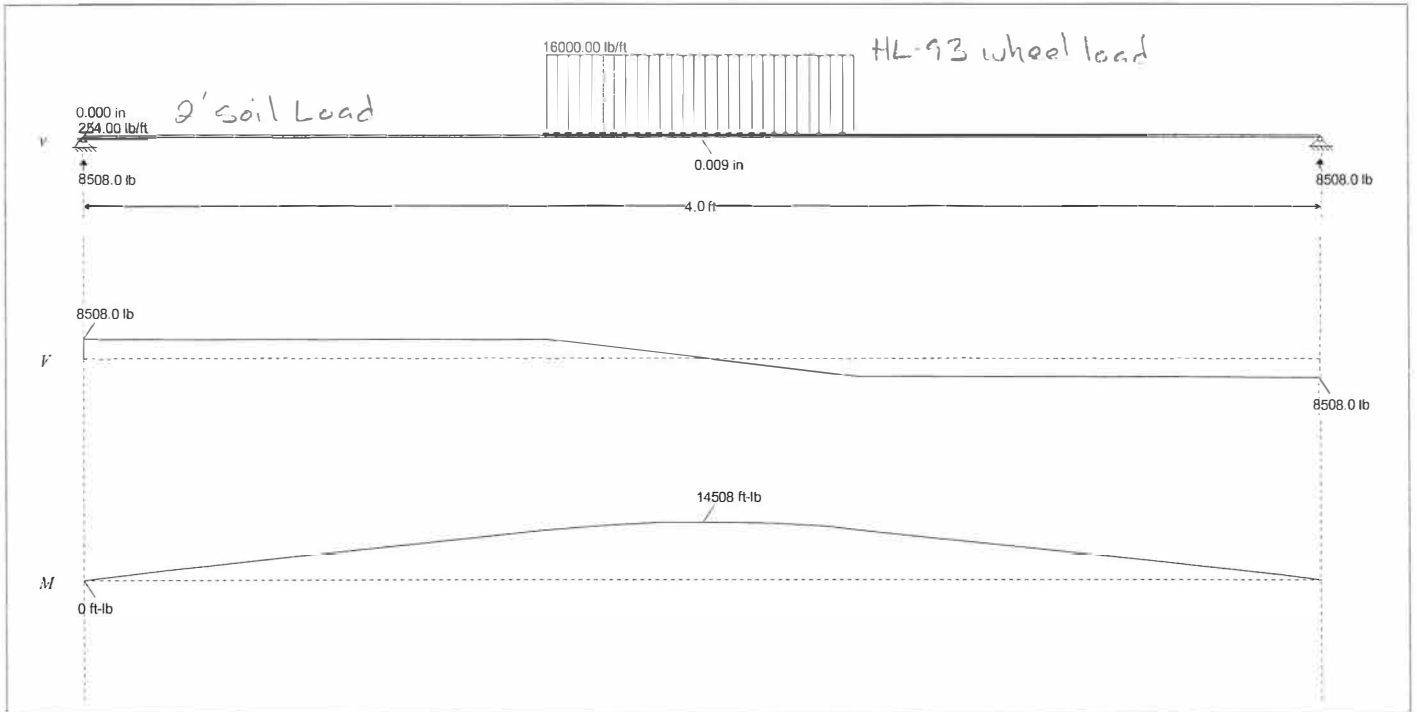
Bar Number	3		
Number of Bars	12		
db	0.375	in	
As per bar	0.11	sq in	
Ast (total)	1.32	sq in	
Length	60	in	
Width	60	in	
Int width	48	in	
Ag	108	sq in	
$\rho = A_{st}/A_g$	0.012		Per ACI 10.9, Must be between 0.01 to 0.08
$\phi$	0.7		
$\phi * P_n = 0.8 * \phi * [0.85 * f'_c * (A_g - A_{st}) + f_y * A_{st}]$	222	kips	OK ACI-318 Eq. 10-2
Rating Factor RF	7.6		AASHTO eqn 13.1.1A-1

**Check Slenderness Effects**

Effective length factor, k	2		
Unsupported length, lu	4.5	ft	
Radius of gyration, r	76.8	in	Per ACI 10.10.1.2, equal to 0.3x dimension
Check $k * l_u / r < 22$	1.41		OK ACI-318 Eq. 10-6

**Check Concrete for Shear**

$\phi$	0.75		
b	60	in	
d	57.81	in	
$f'_c$	3500	psi	
$\phi V_c = \phi [2 * (1 + N_u / 2000 A_g) * f'_c^{0.5} * b * d]$	309	kips	OK ACI-318 Eq. 11-4



Beam Parameters: Length = 4.0 ft, E = 29000.0 ksi, I = 140.0 in<sup>4</sup>, A = 6.0 in<sup>2</sup>

A36 plate  $F_y = 36 \text{ ksi}$ ,  $f_y = 22 \text{ ksi}$  (ASD)

$$f_b = \frac{m}{S} \quad S_{min} = \frac{m}{f_b} = \frac{14508}{22000} \cdot 12 = 7.91 \text{ in}^3$$



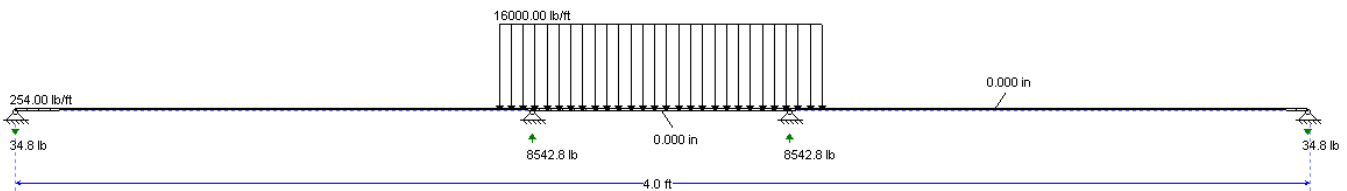
4'x4' plate

find req'd thickness

$$S = \frac{bh^2}{6}$$

$$h = \frac{7.91(6)}{48''} = .99'' \Rightarrow 1'' \text{ plate req'd}$$

Note: steel plates as-built are 1/2" thick. 2ea. 8.5 kip shoring posts will be implemented rather than replacing 1/2" plates with 1" plates.



---

# APPENDIX

---

---

## *Inspection*

---

Agency: Washington State

Program Mgr: Sonia L. Lowry

CD Status: Work

Release Date:

Structure No. V001

SID XG180500

Structure Name Drainge vault

Carrying

Route On

Mile Post

Intersecting

Route Under

Mile Post

2/9/2028

3/18/2028

Inspector's Signature JLL

Cert # G1805

Cert Exp Date

Co-Inspector's Signature

**Current Inspections Performed**

Report Type	Subtype	Rsk Mthd	Begin Date	Comp Date	Interval	Due Date	Hours	Inspector	Cert No	Co-Insp
Initial		1	3/13/2025	3/13/2025			1.0	JLL	G1805	
Routine Bridge		1	3/13/2025	3/13/2025			1.0	JLL	G1805	

**Component Condition Ratings**

**Appraisal**

**Miscellaneous Fields**

G	Overall Condition Classification (BC12)			Scour Critical (NBI Disc) (1680)	1996	Year Built (BW01)	
N	FHWA Deck Overall (BC01)	N		Scour Vulnerability (BAP03)		Asphalt Depth (WIE30)	
N	WSDOT Deck Overall (WC01)	X		Scour Plan of Action (BAP04)	0.00	Design Curb Height (WIE31)	
N	Bridge Railings (BC05)			Waterway (NBI Disc) (1662)	0.00	Bridge Rail Height (WIE32)	
N	Bridge Railing Transitions (BC06)	N		Overtopping Likelihood (BAP02)	1	Number of Utilities (WIE33)	
N	Bridge Joints (BC08)			Apr Roadway Align (BAP01)	Y	Subject to NBIS (WIE34)	
N	Superstructure Overall (BC02)			Fatigue Details (BIR02)	03/17/2025	Inspn QA Date (BIE09)	
N	NSTM Inspection (BC14)			Seismic Vulnerability (BAP05)			
N	Bridge Bearings (BC07)	<b>Optional Condition Ratings</b>					<b>Inspection Flags</b>
N	Substructure Overall (BC03)	6		Drain Condition (LP01)		Soundings (WIE20)	
N	UW Inspection (BC15)	9		Retaining Wall Condition (LP02)		Clearance (WIE21)	
8	Culvert Overall (BC04)					P	PhotosFlag (WIE23)
N	Scour Condition (BC11)					Y	Roadside Hardware Flag (WIE25)
N	Channel Condition (BC09)					Y	QA Flag (WIE24)
N	Channel Protection (BC10)						
	Chan/Prot (NBI Disc) (1677)						
	Pier/Abut/Prot (NBI Disc) (1679)						

**BMS Elements**

Element	Element Description	Total	Units	CS 1	CS 2	CS 3	CS 4
<b>Culvert Elements</b>							
241	Concrete Culvert	285	LF	285	0	0	0

**Notes**

**Culvert Notes**

241 This is a drainage detention vault running along the median area of I-405 near Exist 26, north of 228th St. SE., Bothell, WA . The actual length of culvert is approximately 285 feet, and the vault interior width and height are approximately 20 x 9 feet . The inspection was performed by entering the vault through one of the hatches at night around 11:30 pm on March 12, with one lane I-405 closure. The ground above the vault was not inspected due to the night condition. At the hatch opening, the ground is about 4 feet above the vault. The vault bottom has standing water due to rain on the inspection day. The vault is an active drainage structure with three cells, an inlet chamber, a settling chamber, and an outlet chamber connecting to outfall. the structure condition is good, with typical longitudinal hairline cracks at each expansion joint. The expansion joint spaces at 10 feet, all expansion joints and hatches leak significantly.

Agency: Washington State

Program Mgr: Sonia L. Lowry

CD Status: Work

Release Date:

**Structure No.** V001      **SID** XG180500      **Structure Name** Drainge vault  
**Carrying**      **Route On**      **Mile Post**  
**Intersecting**      **Route Under**      **Mile Post**

Repairs						
Repair No	Pr	R	Repair Descriptions	BMS	Noted	Verified
			(No repairs for this structure)			

**All Inspections and Resources Required**

Report Type	Subtype	Rsk Mthd	Begin Date	Comp Date	Interval	Due Date	Hours	Inspector	Cert No	Co-Insp
Initial		N	3/13/2025	3/13/2025			1.0	JJL	G1805	
<b>Inspection Note</b> Mid night underground inspection, rainy			<b>Late Inspection Explanation</b>			<b>Late PM Resp Date</b>	<b>Late PM Approval</b>	<b>Insp QC Date</b>	<b>Inspn Data Update Date</b>	

Report Type	Subtype	Rsk Mthd	Begin Date	Comp Date	Interval	Due Date	Hours	Inspector	Cert No	Co-Insp
Routine Bridge		N	3/13/2025	3/13/2025			1.0	JJL	G1805	
<b>Inspection Note</b> Mid night underground inspection, rainy			<b>Late Inspection Explanation</b>			<b>Late PM Resp Date</b>	<b>Late PM Approval</b>	<b>Insp QC Date</b>	<b>Inspn Data Update Date</b>	



















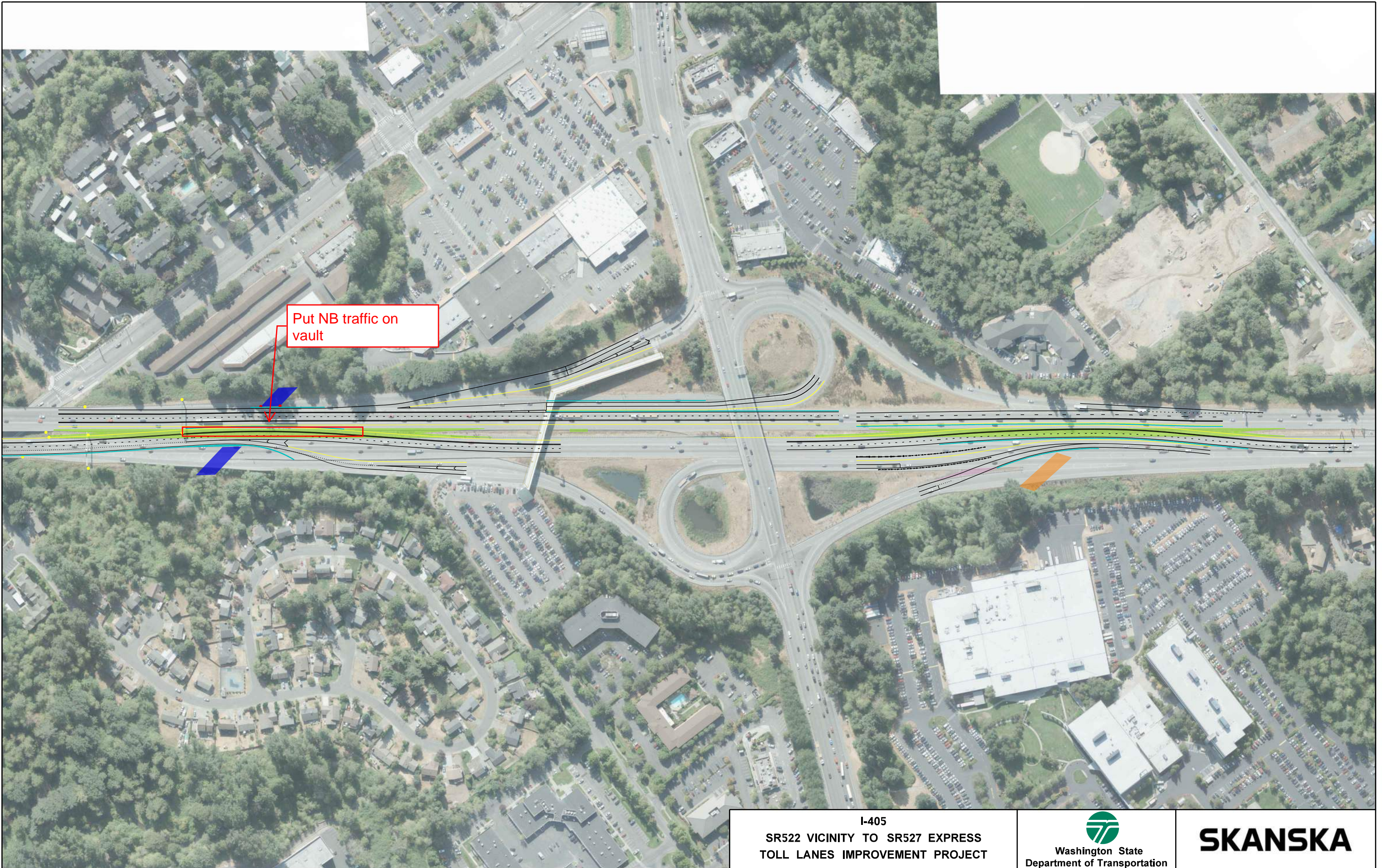


---

# *Plans*

---

\$\$\$\$\$DESIGNFILENAME\$\$\$\$\$  
\$USERNAM\$\$ \$\$\$\$DATE\$\$\$ \$TIMES

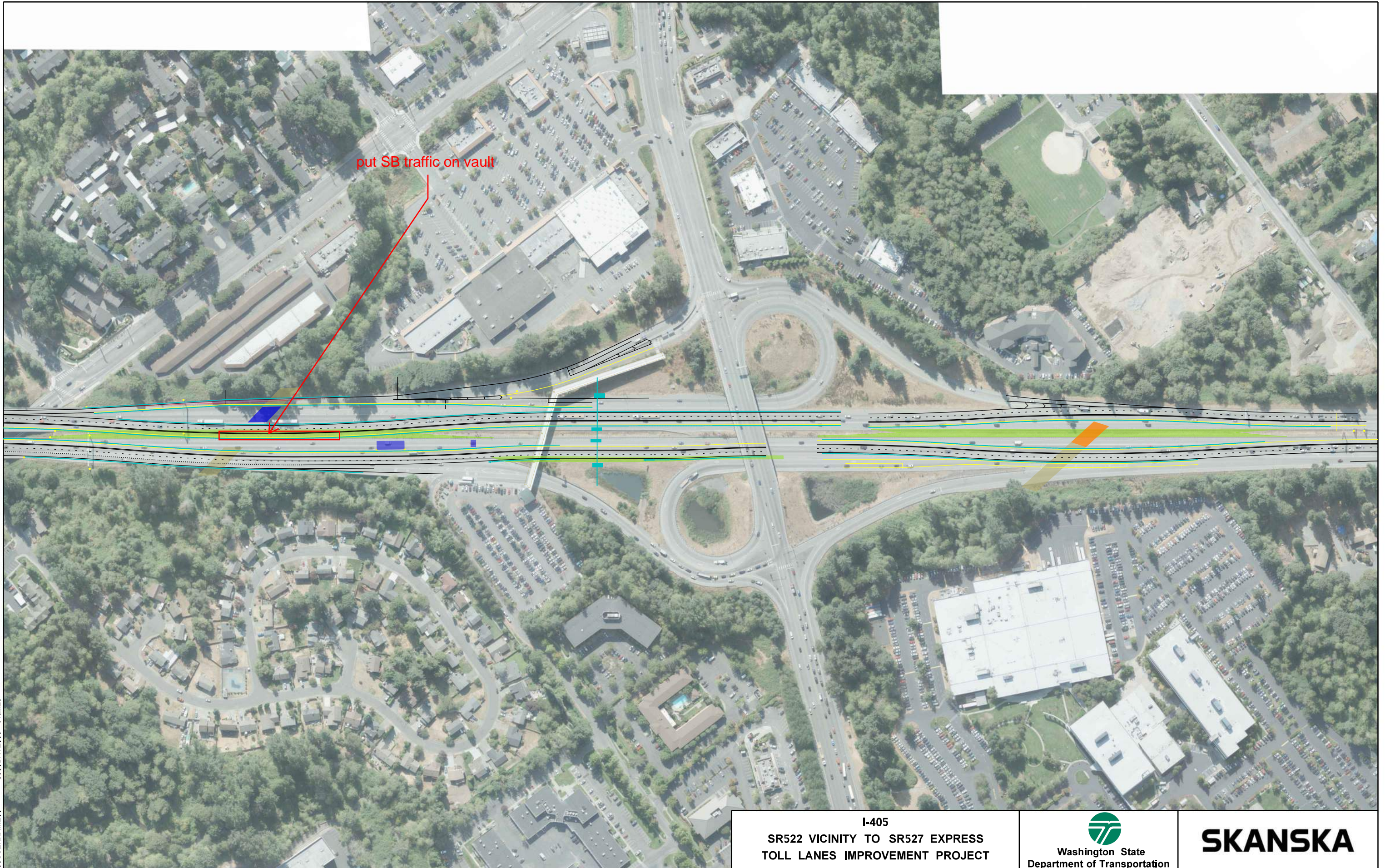


Put NB traffic on vault

I-405  
SR522 VICINITY TO SR527 EXPRESS  
TOLL LANES IMPROVEMENT PROJECT



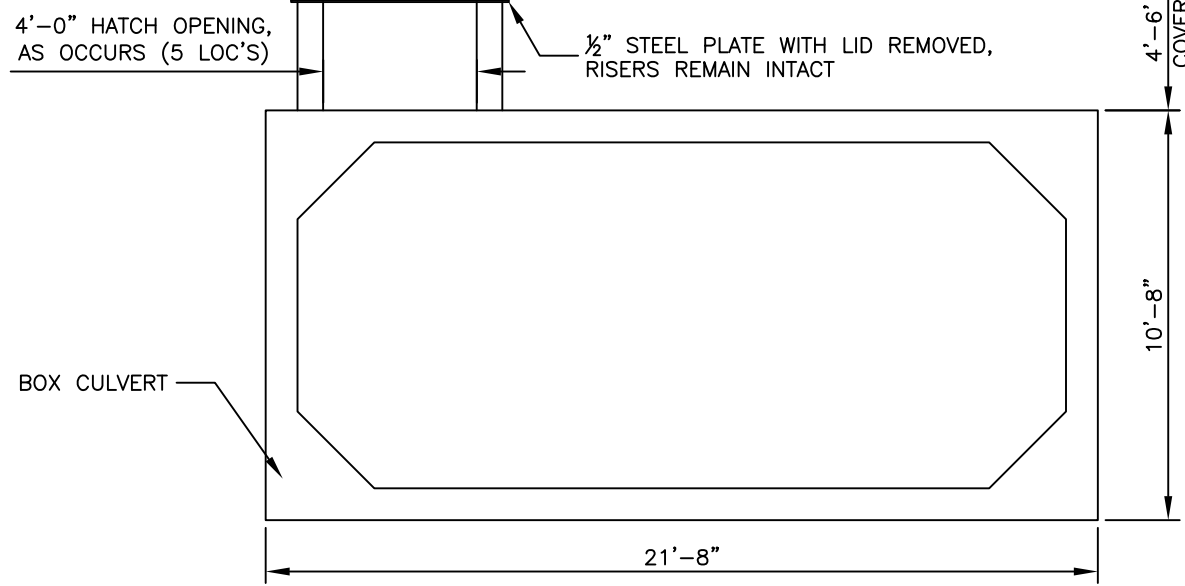
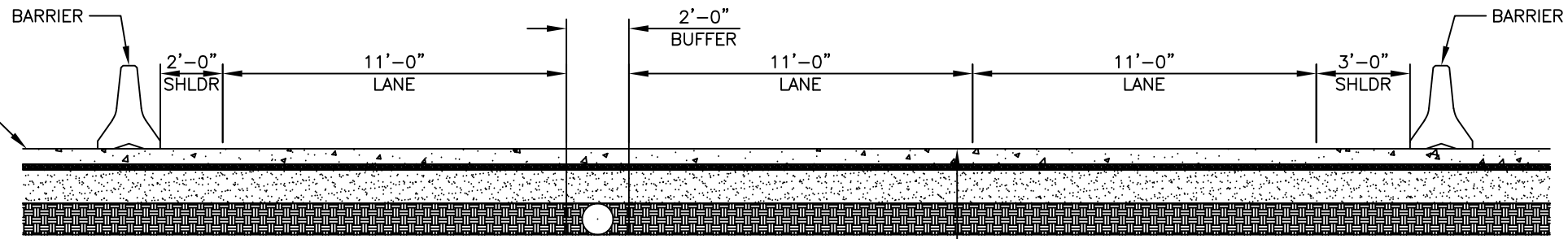
\$\$\$\$\$DESIGNFILENAME\$\$\$\$\$  
\$USERNAM\$\$ \$\$\$\$DATE\$\$\$ \$TIMES



I-405  
SR522 VICINITY TO SR527 EXPRESS  
TOLL LANES IMPROVEMENT PROJECT



6" PERVIOUS ASPHALT LAYER  
 2" CHOKER COURSE  
 13" BASE COURSE/BALLAST  
 12" UNDERDRAIN/NATIVE LAYER



TYP SECTION THROUGH VAULT NW-12  
 SCALE: 1:5



PLANS PREPARED BY  
**4M ENGINEERING**  
 CIVIL - STRUCTURAL  
 6675 PURPLE POPPY LN., PARK CITY, UT 84098  
 801-380-0562  
 WWW.4MENGINEERS.COM  
 DESIGNED BY: JESSICA MERRELL  
 PLANS PREPARED FOR:  
 SKANSKA USA CIVIL  
 18911 NORTH CREEK PKWY, STE 300

PROJECT INFORMATION			
PROJECT TITLE: I-405 BRICKYARD TO SR527			
OWNER: WASH DOT			
DIST	COUNTY	ROUTE	POST MILE
-	SNOHOMISH	405	-
CONTRACT NO.: 9727			

SHEET NAME: TYP SECTION @ VAULT NW-12	
STR NAME: VAULT NW-12	
SHEET 1	STR NO.: VAULT NW-12
OF 1	FILE: Bothell culvert section.dwg

REVISIONS	
DATE	DESCRIPTION
0	5-16-25 ISSUED FOR CONSTRUCTION
-	-
-	-
-	-
-	-
-	-
-	-
-	-
-	-

6/3/25

---

## *Field Investigations*

---

**Re: Box Culvert Findings**

---

**From** Lucarelli, Zachary <Zachary.Lucarelli@skanska.com>  
**Date** Tue 4/15/2025 2:50 PM  
**To** Forrest Megargel <forrestm@4mengineers.com>  
**Cc** Jessica Merrell <jessicam@4mengineers.com>

Forrest,

Our superintendent verified the following today:

"The wall portion is #5 bar 5" OC vertical and #5 bar 10" OC horizontal. The lid portion looks to be #7 bar transverse at 5" OC, and #5 bar longitudinal at 10" OC."

Thanks!

**Zach**

---

**From:** Lucarelli, Zachary  
**Sent:** Monday, April 14, 2025 1:47 PM  
**To:** Forrest Megargel  
**Cc:** Jessica Merrell  
**Subject:** Re: Box Culvert Findings

Forrest,

Some photos attached.

Thanks,

**Zach**

---

**From:** Forrest Megargel <forrestm@4mengineers.com>  
**Sent:** Wednesday, April 2, 2025 6:24 AM  
**To:** Lucarelli, Zachary <Zachary.Lucarelli@skanska.com>  
**Cc:** Jessica Merrell <jessicam@4mengineers.com>  
**Subject:** Box Culvert Findings

**Re: Box Culvert**

---

**From** Lucarelli, Zachary <Zachary.Lucarelli@skanska.com>  
**Date** Thu 4/24/2025 9:49 AM  
**To** Forrest Megargel <forrestm@4mengineers.com>  
**Cc** Jessica Merrell <jessicam@4mengineers.com>

Forrest,

The exterior mat of the walls is #7 verticals at 5" OC, and #5 horizontals at 10" OC.

Thanks,

**Zach**

---

**From:** Forrest Megargel <forrestm@4mengineers.com>  
**Sent:** Thursday, April 17, 2025 7:49 AM  
**To:** Lucarelli, Zachary <Zachary.Lucarelli@skanska.com>  
**Cc:** Jessica Merrell <jessicam@4mengineers.com>  
**Subject:** Box Culvert

Zach,

Based on as-built the bar information we recommend adding shoring to the box culvert, unless the exterior bars in the walls can be verified as #7's or larger. I don't know how practical getting that information would be.

Forrest Megargel, P.E.



6675 Purple Poppy Ln  
Park City, Utah, 84098  
801-380-0562

# Ceiling Rebar



Network: Mar 13, 2025 at 1:14:08 AM PDT  
Local: Mar 13, 2025 at 1:14:08 AM PDT  
N 47° 47' 33.121", W 122° 12' 35.475"  
1-405 S  
Bothell WA 98021  
United States





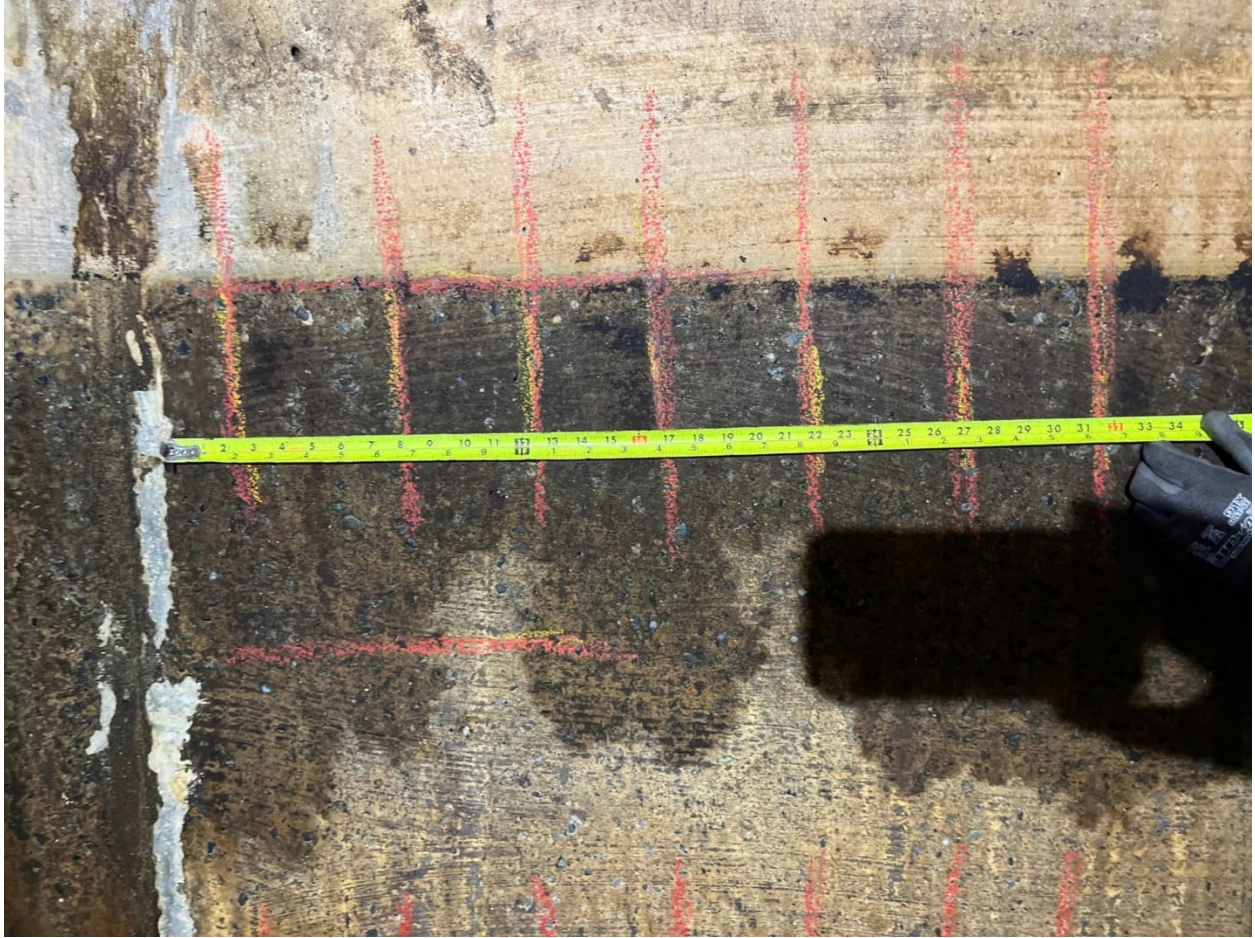


# Wall Rebar

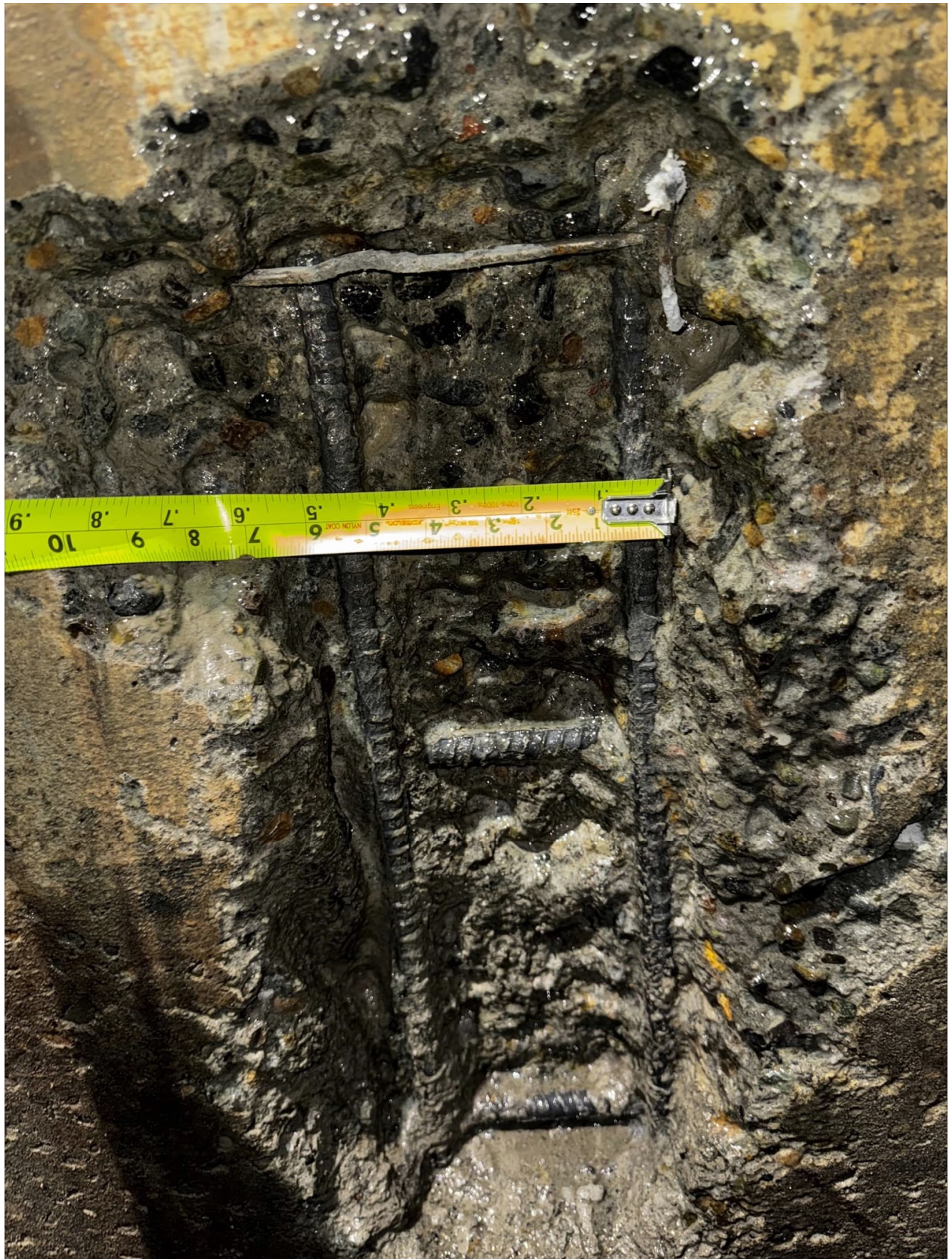












---

## *Sample Plans*

---

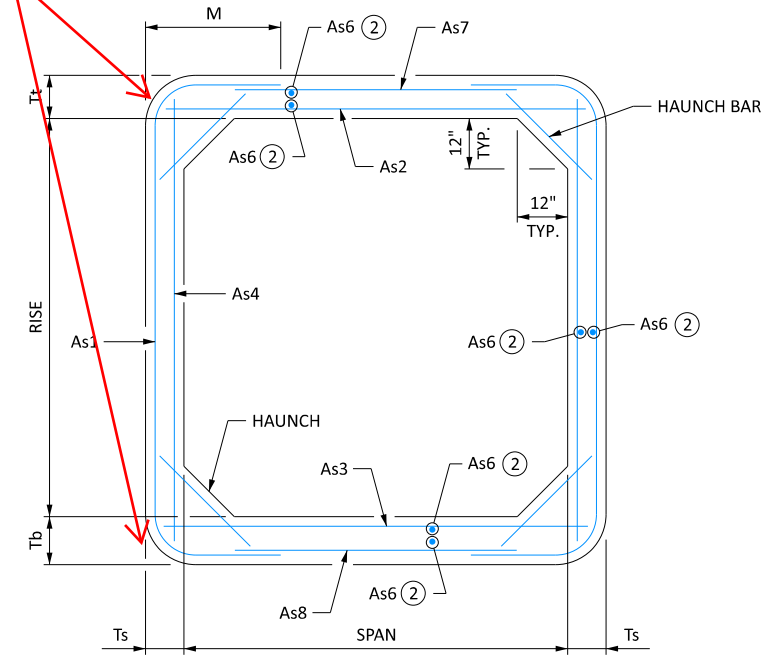
As3 exceeds As2

As7 and As8 bars exceed longitudinal bars

Corner bars match exterior wall rebar (one bar used)

Note: all longitudinal bars are equivalent

SIZE SPAN x RISE (ft.)	CLASS	f'c (psi)	FILL HEIGHT RANGE (ft.)	Tt (in.)	Tb (in.)	Ts (in.)	WEIGHT (lbs./ft.)	REINFORCEMENT REQUIREMENTS ①										
								As1			As2		As3		As4		As7/As8	
								As	LENGTH	M	As	LENGTH	As	LENGTH	As	LENGTH	As	LENGTH
16x4	1	5000	<3	10	11	9	5800	1.33	16'-11"	5'-10"	0.87	16'-6"	0.81	16'-6"	0.22	4'-6"	0.27	10'-5"
	2	5000	3 - 6	10	11	9	5800	1.24	15'-7"	5'-2"	0.83	16'-6"	0.81	16'-6"	0.22	4'-6"	0.27	11'-5"
	3	5000	6 - 10	10	11	10	5950	1.48	17'-4"	6'-1"	1.01	16'-6"	1.00	16'-6"	0.24	4'-6"	0.27	10'-5"
	4	6000	10 - 16	12	12	11	6750	1.85	16'-8"	5'-7"	1.30	16'-6"	1.32	16'-6"	0.27	4'-6"	0.29	11'-1"
16x5	1	5000	<3	10	11	9	6025	1.23	17'-7"	5'-8"	0.95	16'-6"	0.90	16'-6"	0.22	5'-6"	0.27	10'-5"
	2	5000	3 - 6	10	11	9	6025	1.14	16'-3"	5'-0"	0.91	16'-6"	0.90	16'-6"	0.22	5'-6"	0.27	11'-5"
	3	5000	6 - 10	10	11	10	6200	1.36	17'-4"	5'-7"	1.09	16'-6"	1.11	16'-6"	0.24	5'-6"	0.27	11'-3"
16x6	1	5000	<3	10	11	9	6250	1.15	17'-3"	5'-0"	1.01	16'-6"	0.98	16'-6"	0.22	6'-6"	0.27	11'-5"
	2	5000	3 - 6	10	11	9	6250	1.06	17'-0"	4'-11"	0.98	16'-6"	0.98	16'-6"	0.22	6'-6"	0.27	11'-5"
	3	5000	6 - 10	10	11	9	6250	1.38	18'-1"	5'-5"	1.27	16'-6"	1.32	16'-6"	0.22	6'-6"	0.27	11'-5"
	4	6000	10 - 16	12	12	10	7100	1.69	16'-10"	4'-8"	1.66	16'-6"	1.69	16'-6"	0.24	6'-6"	0.29	12'-9"
16x7	1	5000	<3	10	11	8	6250	1.13	16'-10"	4'-4"	1.17	16'-6"	1.16	16'-6"	0.20	7'-6"	0.27	12'-9"
	2	5000	3 - 6	10	11	8	6250	1.05	16'-6"	4'-2"	1.14	16'-6"	1.16	16'-6"	0.20	7'-6"	0.27	12'-10"
	3	5000	6 - 10	10	11	9	6475	1.29	17'-5"	4'-7"	1.34	16'-6"	1.41	16'-6"	0.22	7'-6"	0.27	12'-10"
	4	6000	10 - 16	12	12	10	7350	1.57	17'-10"	4'-8"	1.76	16'-6"	1.80	16'-6"	0.24	7'-6"	0.29	12'-9"
16x8	1	5000	<3	10	11	8	6450	1.05	17'-6"	4'-2"	1.23	16'-6"	1.23	16'-6"	0.20	8'-6"	0.27	12'-9"
	2	5000	3 - 6	10	11	8	6450	0.97	17'-2"	4'-0"	1.20	16'-6"	1.23	16'-6"	0.20	8'-6"	0.27	12'-9"
	3	5000	6 - 10	10	11	9	6700	1.20	18'-2"	4'-6"	1.41	16'-6"	1.50	16'-6"	0.22	8'-6"	0.27	12'-10"
	4	6000	10 - 16	12	12	10	7600	1.47	18'-10"	4'-8"	1.84	16'-6"	1.89	16'-6"	0.24	8'-6"	0.29	12'-9"
16x9	1	5000	<3	10	11	8	6650	0.98	18'-4"	4'-1"	1.29	16'-6"	1.28	16'-6"	0.20	9'-6"	0.27	12'-9"
	2	5000	3 - 6	10	11	8	6650	0.90	17'-11"	3'-10"	1.24	16'-6"	1.28	16'-6"	0.20	9'-6"	0.27	12'-9"
	3	5000	6 - 10	10	11	9	6925	1.13	18'-11"	4'-4"	1.53	16'-6"	1.57	16'-6"	0.22	9'-6"	0.27	12'-9"
	4	6000	10 - 16	12	12	10	7850	1.36	19'-8"	4'-7"	1.90	16'-6"	1.97	16'-6"	0.24	9'-6"	0.29	12'-9"
16x10	1	5000	<3	10	11	8	6850	0.93	19'-1"	3'-11"	1.34	16'-6"	1.34	16'-6"	0.20	10'-6"	0.27	12'-9"
	2	5000	3 - 6	10	11	8	6850	0.84	18'-9"	3'-9"	1.29	16'-6"	1.34	16'-6"	0.20	10'-6"	0.27	12'-9"
	3	5000	6 - 10	10	11	9	7150	1.07	19'-8"	4'-3"	1.58	16'-6"	1.64	16'-6"	0.22	10'-6"	0.27	12'-10"
	4	6000	10 - 16	12	12	10	8100	1.29	20'-6"	4'-6"	1.96	16'-6"	2.06	16'-6"	0.24	10'-6"	0.29	12'-9"
16x11	1	5000	<3	10	11	8	7050	0.91	20'-0"	3'-11"	1.39	16'-6"	1.39	16'-6"	0.20	11'-6"	0.27	12'-9"
	2	5000	3 - 6	10	11	8	7050	0.83	19'-8"	3'-9"	1.33	16'-6"	1.39	16'-6"	0.20	11'-6"	0.27	12'-9"
	3	5000	6 - 10	10	11	9	7375	1.02	20'-6"	4'-2"	1.63	16'-6"	1.70	16'-6"	0.22	11'-6"	0.27	12'-9"
	4	6000	10 - 16	12	12	10	8350	1.23	21'-3"	4'-5"	2.03	16'-6"	2.12	16'-6"	0.24	11'-6"	0.29	12'-9"
16x12	1	5000	<3	10	11	8	7250	0.90	21'-1"	3'-11"	1.43	16'-6"	1.44	16'-6"	0.24	12'-6"	0.27	12'-7"
	2	5000	3 - 6	10	11	8	7250	0.83	20'-9"	3'-9"	1.37	16'-6"	1.44	16'-6"	0.24	12'-6"	0.27	12'-9"
	3	5000	6 - 10	10	11	9	7600	0.99	22'-7"	4'-8"	1.67	16'-6"	1.75	16'-6"	0.24	12'-6"	0.27	11'-7"
	4	6000	10 - 16	12	12	11	8950	1.20	22'-2"	4'-4"	1.92	16'-6"	2.02	16'-6"	0.24	12'-6"	0.29	12'-11"



**GENERAL NOTES**

SEE STANDARD FIG. 5-395.100(A) FOR BASIS OF DESIGN. FILL HEIGHT IS DEFINED AS THE DISTANCE FROM THE TOP OF THE CULVERT TO THE TOP OF THE PAVEMENT OR TO TOP OF FILL IF THERE IS NO PAVEMENT.

DESIGNS FOR FILL HEIGHTS GREATER THAN SHOWN IN THE TABLES ARE AVAILABLE FROM THE MnDOT BRIDGE OFFICE.

SEE STANDARD FIG. 5-395.101(A) AND FIG. 5-397.101(B) FOR ADDITIONAL INFORMATION. TRANSVERSE REINFORCEMENT IS PARALLEL TO THE CULVERT SPAN. LONGITUDINAL REINFORCEMENT IS PERPENDICULAR TO THE CULVERT SPAN.

IF THE FILL HEIGHT RANGE EXTENDS INTO MORE THAN ONE CLASS, USE THE CLASS WITH THE LARGEST REINFORCEMENT AREAS. CHECK MAXIMUM AND MINIMUM FILL HEIGHTS OVER THE FULL AREA OF ROADWAY AND SHOULDERS.

ROADWAY OR SHOULDER FILL HEIGHTS OF LESS THAN 2'-0" REQUIRE A DISTRIBUTION SLAB. EXTEND THE WIDTH OF THE DISTRIBUTION SLAB TO THE OUTSIDE EDGES OF THE ROADWAY SHOULDERS UNLESS DIRECTED BY THE ENGINEER.

USE CONCRETE MIX 3552 FOR THE DISTRIBUTION SLAB.

PLACE 6" THICK CAST-IN-PLACE DISTRIBUTION SLAB WITH NO. 5 BARS AT 1'-0" TRANSVERSELY AND NO. 5 BARS AT 1'-0" LONGITUDINALLY. EPOXY COAT ALL DISTRIBUTION SLAB REINFORCEMENT. CENTER DISTRIBUTION SLAB JOINTS OVER BARREL SEGMENTS. PROVIDE 3" MINIMUM GRANULAR MATERIAL IN ACCORDANCE WITH SPEC. 3149.2B BETWEEN BARREL AND DISTRIBUTION SLAB.

PRECAST DISTRIBUTION SLABS WITH THE SAME REINFORCEMENT MAY BE USED FOR FILL HEIGHTS OVER 1'-0". CENTER DISTRIBUTION SLAB JOINTS OVER BARREL SEGMENTS. PROVIDE 6" MIN GRANULAR MATERIAL IN ACCORDANCE WITH SPEC. 3149.2B BETWEEN BARREL AND DISTRIBUTION SLAB.

REDESIGN DISTRIBUTION SLAB PER THE MnDOT PAVEMENT DESIGN MANUAL IF IT IS USED AS PAVEMENT SURFACE.

CULVERT WEIGHT IS BASED ON 150 P.C.F. WITH A HAUNCH SIZE OF 12 INCHES.

① REINFORCEMENT AREAS ARE IN SQUARE INCHES PER LINEAL FOOT OF BARREL. ALL REINFORCEMENT LENGTHS AND AREAS ARE MINIMUM REQUIREMENTS. REINFORCEMENT REQUIREMENTS ARE FOR WELDED WIRE REINFORCEMENT WITH MINIMUM SPECIFIED YIELD STRESS OF 65 ksi. IF BAR REINFORCEMENT IS SUBSTITUTED FOR WELDED WIRE REINFORCEMENT, INCREASE THE AREA OF REINFORCEMENT BY 8%, AND SUBMIT DESIGN CALCULATIONS VERIFYING COMPLIANCE WITH AASHTO 5.7.3.4 "CONTROL OF CRACKING BY DISTRIBUTION OF REINFORCEMENT".

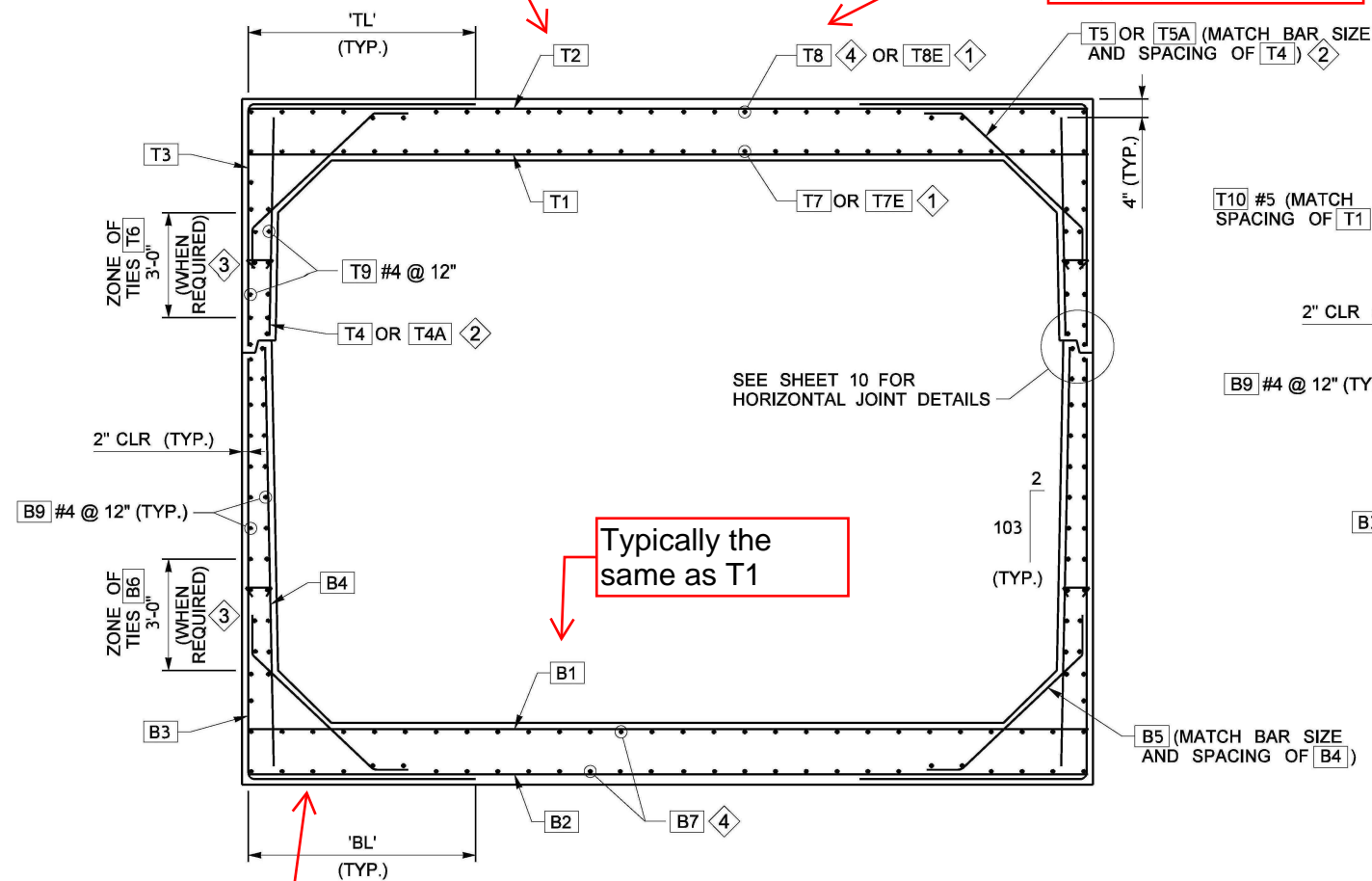
② PLACE LONGITUDINAL REINFORCEMENT DENOTED AS As6 IN ALL SLABS AND WALLS WITH A MINIMUM OF 0.06 IN<sup>2</sup>/FT.

MnDOT  
 REVISION: AUGUST 21, 2024  
 APPROVED: MARCH 24, 2011  
*Nancy Subenberger*  
 STATE BRIDGE ENGINEER

FIG. 5-395.100(E)  
 TITLE: PRECAST CONCRETE BOX CULVERT TABLES  
 DO NOT INCLUDE TABLES WITH PLAN

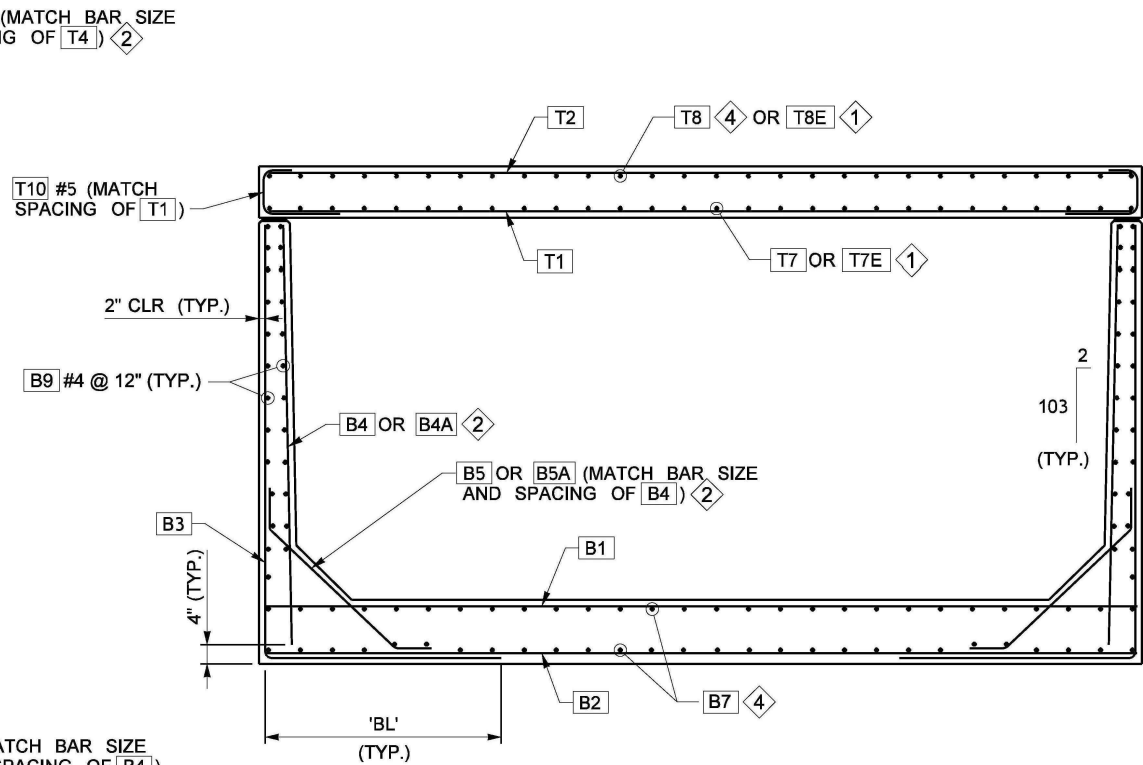
T2 bars exceed longitudinal bars

Note: Longitudinal bars B7 and T8 are equal or better than longitudinal bar T7

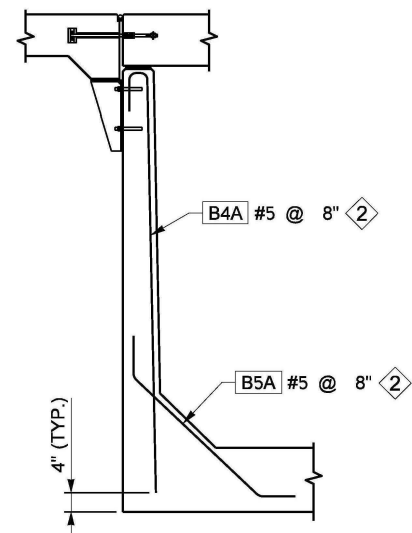


TYPICAL SECTION SPLIT BOX REINFORCEMENT

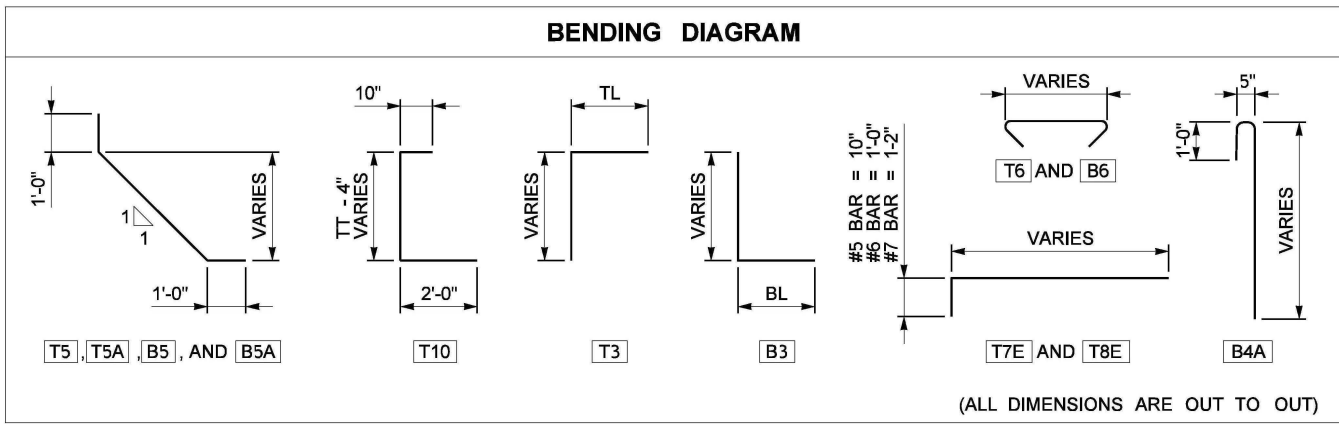
Corner bars match exterior wall rebar (one bar used)



TYPICAL SECTION SPLIT BOX ~ SLAB REINFORCEMENT



SPLIT BOX ~ SLAB ADDITIONAL REINFORCEMENT WHEN APPROACH SLAB SEAT IS PRESENT



KEY NOTES

- 1 BARS T7E AND T8E SHALL BE INSTALLED IN THE END SEGMENTS. ROTATE 90° HOOK AS NECESSARY TO PROVIDE THE SPECIFIED CLEARANCE.  
 SIZE AND SPACING OF BARS T7E SHALL MATCH T7.  
 BARS T8E SHALL BE AS FOLLOWS:  
 END SEGMENT WITHOUT HEADWALL OR TRAFFIC BARRIER: #5 @ 12"  
 END SEGMENT WITH UP TO 2'-0" HEADWALL: #6 @ 12"  
 END SEGMENT WITH UP TO 4'-0" HEADWALL: #6 @ 6"  
 END SEGMENT WITH TRAFFIC BARRIER: #7 @ 6"  
 FOR ADDITIONAL END SEGMENT DETAILS SEE SHEET 11.
- 2 WHEN AN APPROACH SLAB SEAT IS PRESENT, ADDITIONAL REINFORCEMENT IS REQUIRED AS FOLLOWS:  
 FOR SPLIT BOX ~ SLAB STRUCTURES:  
 ADD B4A #5 @ 8" AND B5A #5 @ 8". BUNDLE WITH TYPICAL B4 AND B5 RESPECTIVELY.  
 FOR SPLIT BOX STRUCTURES:  
 ADD T4A #5 @ 8" AND T5A #5 @ 8". BUNDLE WITH TYPICAL T4 AND T5 RESPECTIVELY.
- 3 TIES T6 #4 AND B6 #4 SHALL BE SPACED AT 6" MAX. VERTICALLY AND AT 2'-0" MAX. HORIZONTALLY. EACH TIE SHALL BE HOOKED AROUND LONGITUDINAL BARS T9 OR B9. ADDITIONAL BARS T9 AND B9 MAY BE ADDED TO FACILITATE PLACEMENT OF TIES AS REQUIRED.
- 4 BARS B7 AND T8 SHALL BE #4 @ 12" WHEN CORRESPONDING SLAB THICKNESS ≤ 20 INCHES, AND #4 @ 9" FOR THICKER SLABS.



Sep 12, 2023

BURIED STRUCTURE SPLIT BOX

STANDARD PLAN E-20.10-00

SHEET 4 OF 17 SHEETS

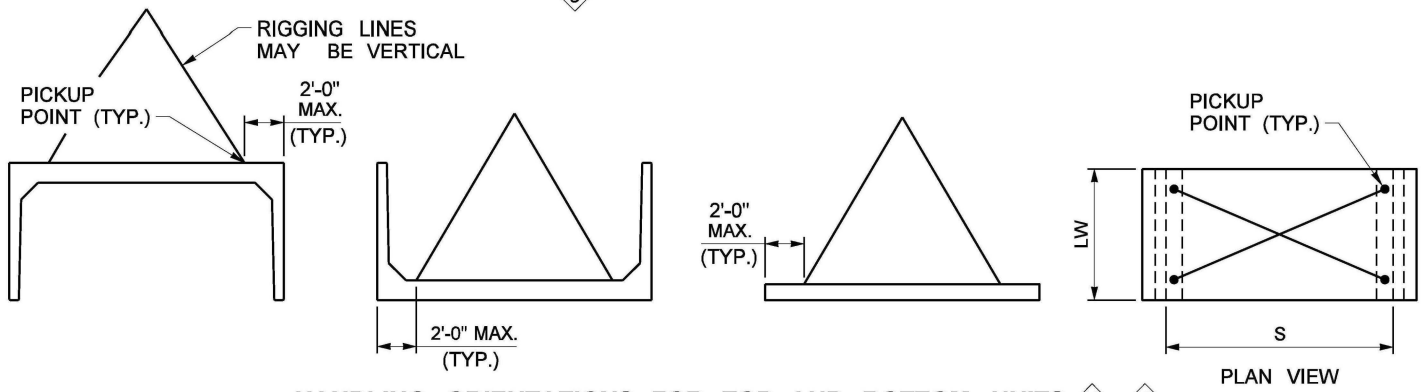
APPROVED FOR PUBLICATION  
 Sep 12, 2023  
 STATE DESIGN ENGINEER  
 Washington State Department of Transportation

DESIGN TABLE ~ CLASS I STRUCTURES ~ SPANS 12', 15' AND 18'

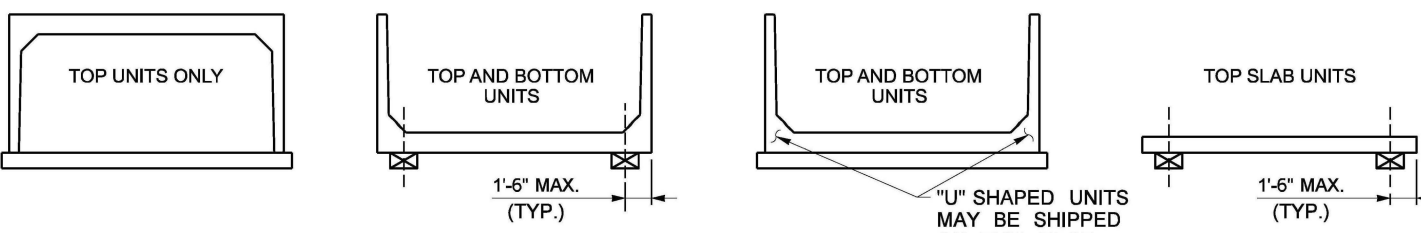
DESIGN SPAN S ①	DESIGN HEIGHT			FILL DEPTH FD ②	MEMBER THICKNESS			TOP UNIT REINFORCEMENT ③										BOTTOM UNIT REINFORCEMENT ④										MATERIAL QUANTITIES				STR. I BEARING DEMAND (PSF) ④	REQ'D HORIZ JOINT TYPE ⑥					
	TOTAL H	TOP UNIT WALL HT	BOT. UNIT WALL HB		WALLS TW	TOP SLAB TT	BOT. SLAB TB	T1 (SLAB INTERIOR)		T2 (SLAB EXTERIOR)		T3 (CORNER)			T4 (WALL INTERIOR)		T6 (TIES) ⑦	T7 (BOT.)		B1 (SLAB INTERIOR)		B2 (SLAB EXTERIOR)		B3 (CORNER)			B4 (WALL INTERIOR)		B6 (TIES) ⑦	TOP UNIT ⑧				BOTTOM UNIT ⑩				
								SIZE	SPA.	SIZE	SPA.	SIZE	SPA.	TL	SIZE	SPA.		SIZE	SPA.	SIZE	SPA.	SIZE	SPA.	BL	SIZE	SPA.	CONC. (CY/FT)	STEEL (LBS/FT)		CONC. (CY/FT)	STEEL (LBS/FT)							
12'	10'	N/A	10'	0' ≤ FD < 2'	10"	12"	10"	#7	6"	#5	12"	N/A			#4	8"	N/A	#5	10"	#6	6"	#7	5"	#7	5"	3'-2"	#4	8"	N/A	0.58	106.1	1.06	322.5	2397	2			
				2' ≤ FD ≤ 4'	10"	12"	10"	#7	6"	#5	12"	#4	8"	#4	12"	#6		6"	#7	5"	#7	5"	3'-2"	#4	8"	0.58	98.4	1.06		322.5	2490	2						
				4' < FD ≤ 6'	12"	12"	12"	#8	6"	#5	12"	#4	8"	#4	12"	#6		6"	#6	5"	#7	5"	4'-3"	#4	8"	0.59	112.8	1.28		318.9	2901	2						
				6' < FD ≤ 8'	12"	12"	12"	#8	6"	#5	12"	#4	8"	#4	12"	#6		6"	#7	5"	#7	5"	3'-4"	#4	8"	0.59	112.8	1.28		327.7	3255	2						
				8' < FD ≤ 10'	12"	12"	12"	#9	6"	#5	12"	#4	8"	#6	10"	#7		6"	#7	5"	#8	5"	3'-8"	#4	8"	0.59	150.3	1.28		382.2	3631	2						
15'	10'	N/A	10'	0' ≤ FD < 2'	10"	12"	10"	#9	6"	#5	12"	N/A			#4	8"	N/A	#4	12"	#8	6"	#6	5"	#7	5"	3'-11"	#4	8"	N/A	0.69	157.2	1.15	361.0	2269	2			
				2' ≤ FD ≤ 4'	10"	12"	10"	#8	6"	#5	12"	#4	8"	#4	12"	#8		6"	#6	5"	#7	5"	5'-1"	#4	8"	0.69	138.3	1.15		378.8	2313	2						
				4' < FD ≤ 8'	12"	14"	12"	#9	6"	#5	10"	#4	8"	#4	12"	#9		6"	#6	5"	#7	5"	4'-1"	#4	8"	0.81	163.6	1.39		399.5	3147	2						
				8' < FD ≤ 10'	12"	16"	14"	#9	6"	#6	12"	#4	8"	#5	10"	#8		6"	#6	5"	#8	5"	3'-7"	#4	8"	0.91	183.0	1.50		422.7	3625	2						
	15'	12' TO 15'	5'	7' TO 10'	0' ≤ FD < 2'	10"	12"	10"	#9	6"	#6	7"	#6	7"	3'-0"	#4	8"	N/A	#5	9"	#8	6"	#5	10"	#6	5"	4'-4"	#4	8"	N/A	0.99	272.1	1.15	301.1	2030	1		
					2' ≤ FD ≤ 4'	10"	12"	10"	#9	6"	#6	7"	#6	7"	3'-0"	#4	8"		#4	12"	#8	6"	#5	12"	#6	6"	4'-9"	#4	8"		0.99	260.1	1.15	282.2	1992	1		
					4' < FD ≤ 8'	10"	14"	12"	#9	6"	#5	10"	#5	5"	5'-2"	#4	8"		#4	12"	#9	6"	#5	10"	#6	5"	3'-9"	#4	8"		1.09	244.9	1.26	315.9	2792	1		
					8' < FD ≤ 12'	12"	16"	14"	#10	6"	#6	12"	#5	6"	3'-10"	#4	8"		#4	12"	#9	6"	#6	12"	#7	6"	3'-5"	#4	8"		1.27	273.3	1.50	342.9	3739	1		
					12' < FD ≤ 16'	12"	18"	16"	#10	6"	#6	12"	#6	6"	3'-9"	#4	8"		#4	12"	#9	6"	#6	10"	#7	5"	3'-7"	#4	8"		1.38	292.3	1.60	375.3	4436	1		
					16' < FD ≤ 20'	12"	20"	18"	#10	6"	#5	6"	#6	6"	3'-9"	#4	8"		#4	12"	#10	6"	#6	12"	#8	6"	3'-9"	#4	8"		1.48	303.5	1.71	417.2	5372	1		
					20' < FD ≤ 24'	12"	22"	22"	#10	6"	#6	10"	#6	6"	3'-11"	#4	8"		Y	#4	12"	#10	6"	#6	9"	#8	6"	3'-11"	#4		8"	Y	1.59	327.1	1.92	443.4	6342	1
					24' < FD ≤ 28'	12"	22"	22"	#11	6"	#6	10"	#7	5"	3'-11"	#4	8"		Y	#4	12"	#10	6"	#6	10"	#8	5"	3'-11"	#4		8"	Y	1.59	387.9	1.92	473.0	7209	1
					28' < FD ≤ 32'	12"	24"	24"	#11	6"	#7	10"	#7	5"	4'-1"	#4	8"		Y	#4	12"	#11	6"	#7	10"	#8	5"	4'-1"	#4		8"	Y	1.69	402.5	2.02	522.3	8145	1
32' < FD ≤ 38'	12"	24"	24"	#11	5"	#7	10"	#8	5"	4'-1"	#4	8"	Y	#4	12"	#11	6"	#7	10"	#8	5"	4'-1"	#4	8"	Y	1.69	470.2	2.02	522.3	9445	1							
18'	10'	N/A	10'	0' ≤ FD < 2'	10"	16"	12"	#8	6"	#6	12"	N/A			#4	8"	N/A	#4	12"	#9	6"	#6	5"	#7	5"	3'-2"	#4	8"	N/A	1.04	164.2	1.37	422.3	2259	2			
				2' ≤ FD ≤ 4'	10"	14"	12"	#9	6"	#5	10"	#4	8"	#4	12"	#9		6"	#6	5"	#7	5"	3'-2"	#4	8"	0.92	188.0	1.37		420.7	2348	2						
				4' < FD ≤ 6'	12"	16"	14"	#9	6"	#6	12"	#4	8"	#4	12"	#10		6"	#7	10"	#7	5"	4'-3"	#4	8"	1.06	195.9	1.63		449.0	2731	2						
				6' < FD ≤ 8'	12"	18"	16"	#9	6"	#6	12"	#4	8"	#4	12"	#9		6"	#7	10"	#7	5"	3'-10"	#4	8"	1.18	196.3	1.75		412.6	3165	2						
				8' < FD ≤ 10'	12"	18"	16"	#10	6"	#6	12"	#4	8"	#4	12"	#9		6"	#6	5"	#8	5"	3'-6"	#4	8"	1.18	196.3	1.75		483.8	3576	2						
	18'	12' TO 15'	5'	7' TO 10'	0' ≤ FD < 2'	10"	14"	12"	#9	6"	#6	9"	#6	9"	3'-1"	#4	8"	N/A	#5	8"	#8	6"	#6	10"	#6	5"	3'-1"	#4	8"	N/A	1.22	290.0	1.37	328.2	1877	1		
					2' ≤ FD ≤ 4'	10"	14"	12"	#9	6"	#5	8"	#6	8"	4'-0"	#4	8"		#4	12"	#9	6"	#6	10"	#6	5"	3'-1"	#4	8"		1.22	272.9	1.37	356.4	2001	1		
					4' < FD ≤ 6'	10"	16"	14"	#9	6"	#5	9"	#5	6"	3'-8"	#4	8"		#4	12"	#9	6"	#5	10"	#7	5"	3'-6"	#4	8"		1.34	261.4	1.49	381.6	2349	1		
					6' < FD ≤ 10'	10"	18"	16"	#10	6"	#6	12"	#6	6"	3'-5"	#4	8"		#4	12"	#10	6"	#6	10"	#7	5"	3'-5"	#4	8"		1.47	316.1	1.61	428.4	3198	1		
					10' < FD ≤ 14'	12"	20"	18"	#11	6"	#5	6"	#5	6"	3'-9"	#4	8"		#4	12"	#10	6"	#6	10"	#7	5"	3'-9"	#4	8"		1.67	360.8	1.87	444.3	3984	1		
					14' < FD ≤ 18'	12"	22"	22"	#11	6"	#5	7"	#6	7"	3'-11"	#4	8"		Y	#4	12"	#10	6"	#6	10"	#7	5"	3'-11"	#4		8"	Y	1.79	380.4	2.12	461.9	4973	1
					18' < FD ≤ 22'	12"	22"	22"	#11	5"	#6	10"	#6	5"	3'-11"	#4	8"		Y	#4	12"	#11	6"	#6	10"	#8	5"	3'-11"	#4		8"	Y	1.79	443.9	2.12	548.0	5841	1
					22' < FD ≤ 30'	12"	24"	24"	#10	4"	#7	10"	#6	5"	4'-1"	#4	8"		Y	#4	12"	#10	4"	#7	10"	#8	5"	4'-1"	#4		8"	Y	1.92	462.7	2.24	610.4	7643	1

KEY NOTES

- ① DESIGN SPAN 'S', SHALL BE TAKEN EQUAL TO THE HORIZONTAL DISTANCE BETWEEN INSIDE FACE OF WALLS AT THE CORNER BETWEEN THE FILLET AND THE WALL AS SHOWN ON SHEET 1. FOR SEGMENTS WITH A SKEW SEE GRAPHICAL CLARIFICATION OF DESIGN SPAN ON SHEET 3. IF THE DESIGN SPAN FALLS IN BETWEEN A DESIGN SPAN VALUE IN THE TABLES, USE REINFORCEMENT FOR THE LONGER SPAN. CLASS 1 STRUCTURES WITH SPANS GREATER THAN 18 FEET AND LESS THAN 20 FEET SHALL USE GEOMETRY AND REINFORCEMENT FOR 21 FOOT SPAN CLASS 2 STRUCTURES WITH A PGA = 0.32G.
- ② THE MAXIMUM FILL DEPTH OVER THE ENTIRE BURIED STRUCTURE SHALL BE USED WHEN SELECTING DESIGN FILL DEPTH.
- ③ FOR REINFORCING DETAILS SEE SHEET 4.
- ④ MAXIMUM REQUIRED BEARING RESISTANCE FOR STRENGTH LIMIT STATE.
- ⑤ THESE STRUCTURES HAVE BEEN DESIGNED FOR A TRAVERSE DIFFERENTIAL SETTLEMENT DISPLACEMENT EQUAL TO 2 INCHES PER 100 FEET OF STRUCTURAL SPAN (DESIGN SPAN + 1.0 FOOT).
- ⑥ FOR HORIZONTAL JOINT TYPE DETAILS SEE SHEET 10.
- ⑦ WALL TIES T6 AND B6 ARE REQUIRED WHEN INDICATED BY LETTER 'Y'.
- ⑧ MATERIAL QUANTITIES ARE FOR A TYPICAL INTERIOR SEGMENT. STEEL WEIGHT DOES NOT INCLUDE ADDITIONAL REINFORCING REQUIRED FOR APPROACH SLAB SEAT.
- ⑨ SINGLE BARS SPACED AT 4 INCHES MAY BE SUBSTITUTED BY TWO-BAR BUNDLES SPACED AT 8".
- ⑩ QUANTITIES OF BOTTOM UNIT CORRESPOND TO 'HB' = 10'-0".
- ⑪ REINFORCING OF PRECAST UNITS HAVE BEEN DESIGNED FOR HANDLING AND SHIPPING ORIENTATIONS PRESENTED ON THIS SHEET. ALTERNATE SHIPPING OR HANDLING ORIENTATIONS SHALL BE ANALYZED BY THE CONTRACTOR.
- ⑫ CONCRETE COMPRESSIVE STRENGTH SHALL BE AT LEAST F<sub>CI</sub> = 3.5 KSI FOR HANDLING AND F<sub>C</sub> = 7.0 KSI FOR SHIPPING.



HANDLING ORIENTATIONS FOR TOP AND BOTTOM UNITS ⑪, ⑫



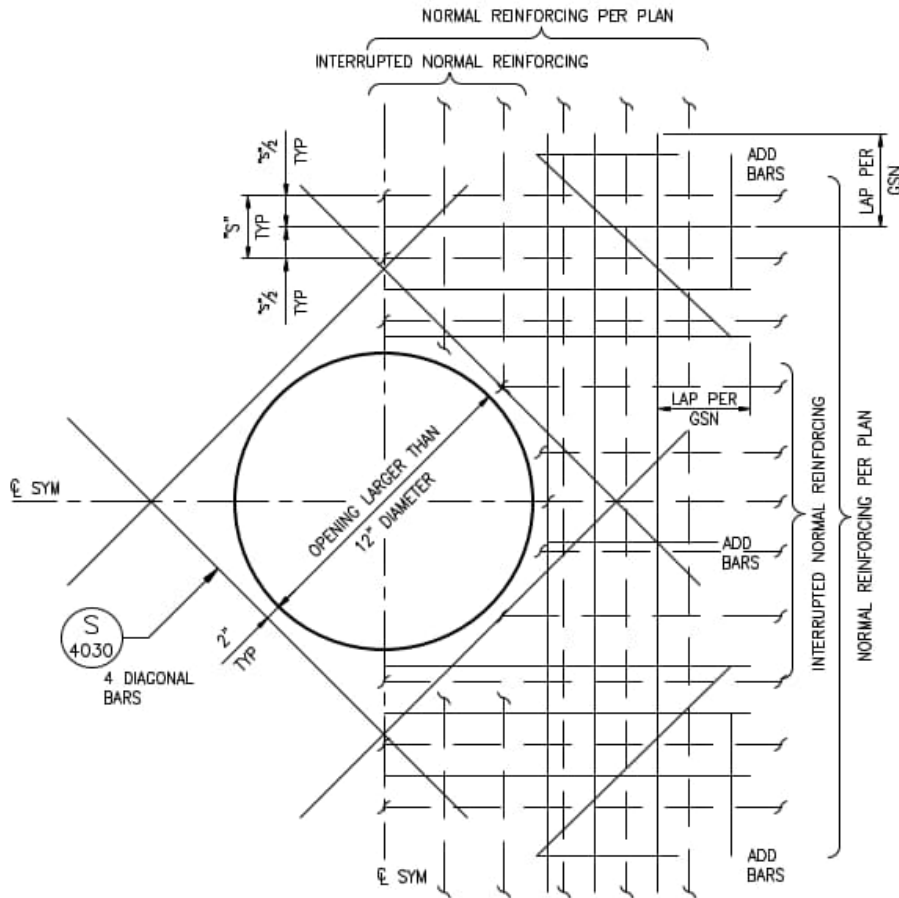
SHIPPING ORIENTATIONS ⑪, ⑫



Sep 12, 2023

**BURIED STRUCTURE  
SPLIT BOX**  
**STANDARD PLAN E-20.10-00**  
SHEET 5 OF 17 SHEETS

APPROVED FOR PUBLICATION  
*Mark A. Davis*  
STATE DESIGN ENGINEER  
Washington State Department of Transportation  
Sep 12, 2023



**NOTES:**

1. THIS DETAIL TO BE USED FOR OPENINGS LARGER THAN 12"Ø AND WHEN CALLED FOR ON THE DRAWINGS OR WHEN NO OTHER ADDITIONAL REINFORCING IS SPECIFIED. FOR OPENINGS SMALLER THAN 12"Ø, USE DETAIL S/4030.
2. FOR OPENINGS LESS THAN 60": AREA OF ADD BARS AT EACH EDGE OF OPENING IN EACH DIRECTION SHALL MATCH ½ THE CROSS SECTIONAL AREA OF THE INTERRUPTED BARS. BARS UP TO TWO BAR SIZES LARGER THAN NORMAL REINFORCING MAY BE USED. FIT ADD BARS WITHIN A DISTANCE OF 2X WALL/SLAB THICKNESS FROM EDGE OF OPENING.  
  
FOR OPENINGS 60" AND LARGER: OMIT VERTICAL AND HORIZONTAL ADD BARS AND USE (4) #6 BARS FOR DIAGONAL BARS SIMILAR TO DETAIL S/4030.
3. CUT NORMAL REINFORCING 2" CLEAR OF OPENING.
4. PROVIDE STANDARD ACI HOOKS ON BARS/DOWELS IF STRAIGHT EXTENSION PAST THE OPENING CANNOT BE ACHIEVED.
5. PLACE ADD BARS IN SAME PLANES AS NORMAL REINFORCING INDICATED.
6. PLACE #5 ADD DIAGONAL CORNER BARS UNDER NORMAL REINFORCING INDICATED.
7. WHEN AN INTERSECTING SLAB OR WALL OCCURS WITHIN ONE WALL/SLAB THICKNESS OF THE EDGE OF OPENING, NO ADD BARS ARE REQUIRED ON THAT SIDE.

**ADDITIONAL REINFORCING AT CIRCULAR OPENINGS IN WALLS/SLABS**

NOT TO SCALE





I-405 NB

ITS #103

1

2

3

4

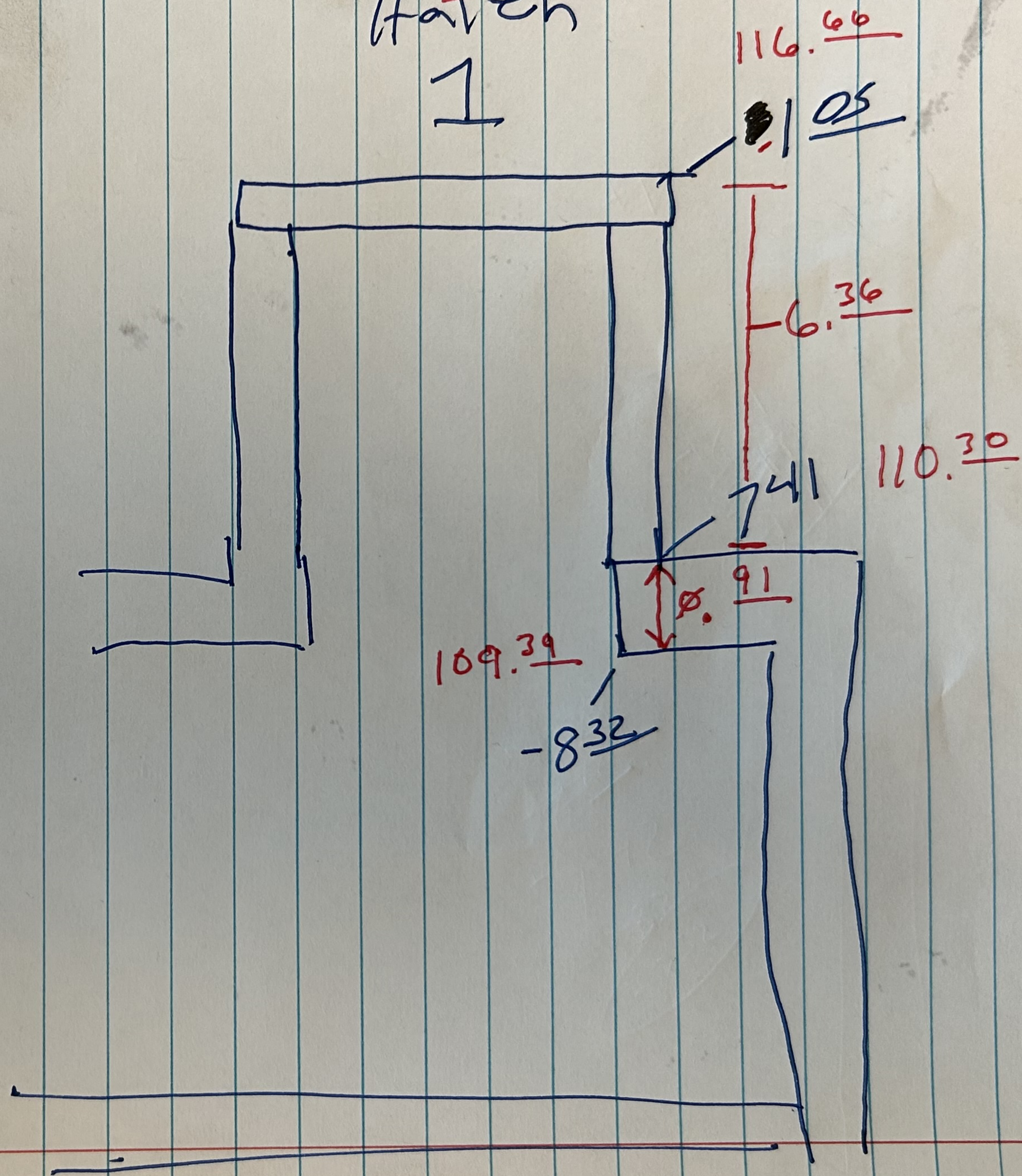
5

6

7

I-405 SB

North End  
Hatch  
1



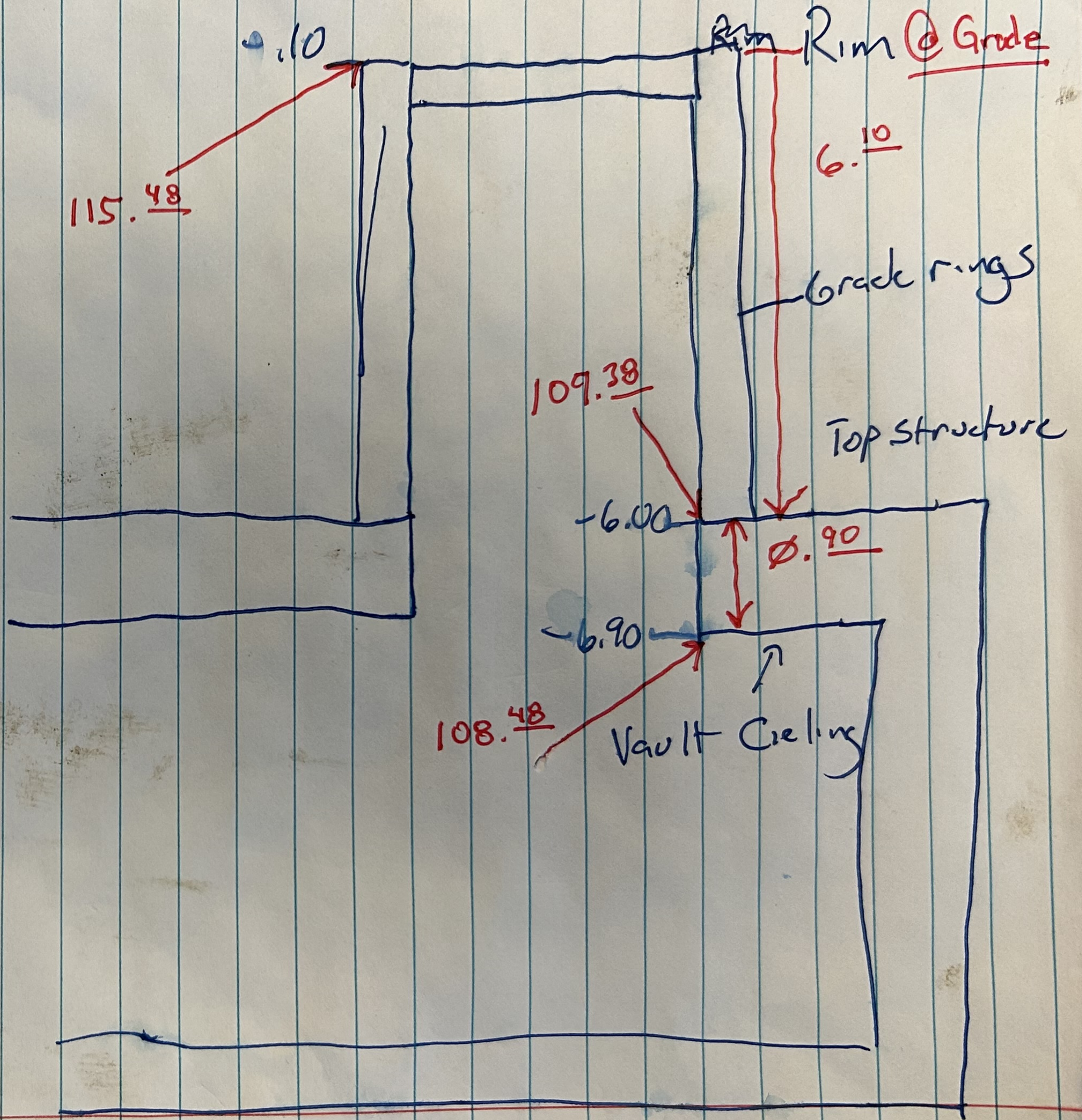
IT

117.71

250317 PRKER 120

115.38 per survey shot  
 0.00  
 ITS  
 25031 7 PRKER 103

Hatch 6



May 15, 2025 at 2:00:35 AM  
I-405 S  
Bothell WA 98021  
United States

